

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 12-18-84					
Company Conoco, Inc.					Connection EPN/G					
Pool Skaggs Abo Gas					Formation Abo					
Completion Date 6-28-84					Total Depth 7503'		Plug Back TD 7452'		Elevation 3579.6'GL	
Farm or Lease Name Skaggs B					Unit B					
Csg. Size 7"	Wt. 26 #	d 6.276	Set At 7500'	Perforations: From 7042' To 7411'					Well No. 7	
Tbg. Size 2 3/8"	Wt. 4.6 #	d 1.995	Set At 7021'	Perforations: From Open To Ended					Unit Sec. Twp. Rge. B 12 20 37E	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Dual - Gas & Oil					Packer Set At 7000'					County Lea
Producing Thru Tubing		Reservoir Temp. °F 140° 6999'		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2			State New Mexico	
L 6999'	H 6999'	Gg 0.663	% CO ₂ 0.307	% N ₂ 3.488	% H ₂ S 0.000	Prover —	Meter Run 4.026"	Taps Flange		

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
SI							1650	44		
1.	4.026" X 1.500"			125	11.25	90	1563	59		
2.	4.026" X 1.500"			128	12.00	74	1485	60		
3.	4.026" X 1.500"			150	54.00	88	1362	62		
4.	4.026" X 1.500"			510	30.50	91	1144	65		
5.										

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	10.84	39.430	138.2	0.9723	1.228	1.011	516
2	10.84	41.163	141.2	0.9868	1.228	1.012	547
3	10.84	93.877	163.2	0.9741	1.228	1.014	1234
4	10.84	126.323	523.2	0.9715	1.228	1.043	1704
5							

NO.	P _t	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1.	0.21	550	1.49	0.978	33.34/6	
2.	0.21	534	1.45	0.977	A.P.I. Gravity of Liquid Hydrocarbons 46° E 60°F	Deg.
3.	0.25	548	1.48	0.973	Specific Gravity Separator Gas 0.663	XXXXXXX
4.	0.79	551	1.49	0.919	Specific Gravity Flowing Fluid XXXXX	
5.					Critical Pressure 663.7	P.S.I.A.
					Critical Temperature 369.2	P.S.I.A.

P _c 1633	P _c 2666.7		
NO.	P _t ²	P _w	P _w ²
1*	3850.2	1571	2468.0
2	3542.7	1508	2274.1
3	2911.1	1372	1882.4
4	2208.8	1202	1444.8
5	4219.7 (SI BHP)		

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.182$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2527.7$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.659$

Absolute Open Flow	2,828	Mcf/d @ 15.025	Angle of Slope @	57°	Slope, n	0.649
Remarks: * BHP were measured @ 6999'. Well produced 5 bbls. of oil during test.						
Approved By Commission:	Conducted By: T.C. Aduddell Don Bennett	Calculated By: Tom C. Aduddell	Checked By:			

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O. C. D.
HOBBS OFFICE

WORK SHEET FOR CALCULATION OF WELLHEAD PRESSURES (P_c or P_w)

Form C-122F
Adopted 9-1-65

FROM KNOWN BOTTOM HOLE PRESSURE (P_f or P_s)

COMPANY Conoco, Inc. LEASE Skaggs B WELL NO. 7 DATE 12-18-84

LOCATION: Unit B Section 12 Township 20S Range 37E

L 6999' H 6999' L/H 1.000 G 0.7573 % CO₂ 0.307 % N₂ 3.488 % H₂S 0.000

GH 5300 P_{CT} 663.7 T_{CT} 369.2

TABLE IX & X

SIBHA

LINE		1st 1	2nd 2	3rd 3	4	5	6	7	8
1	T _w (W.H. °R)	504	504	504					
2	T _s (B.H. °R)	600	600	600					
3	T = ($\frac{T_w + T_s}{2}$)	552	552	552					
4	Z (Est.)	0.834	0.793	0.784					
5	TZ	460	432	433					
6	GH/TZ	11.522	12.269	12.240					
7	e ^S (Table XIV)	1.540	1.584	1.582					
8	$\frac{P_f}{P_s}$ or P_s	2054.2	2054.2	2054.2					
9	P_f^2 or P_s^2	4219.7	4219.7	4219.7					
10	$P_c^2 = P_f^2 / e^S$ or $P_w^2 = P_s^2 / e^S$	2740.1	2664.0	2667.3					
11	P_c or P_w	1655	1632	1633					
12	$P = (\frac{P_w + P_s}{2})$ or $(\frac{P_c + P_f}{2})$	1854.6	1843.1	1843.6					
13	$P_r = (P / P_{CT})$	2.79	2.78	2.78					
14	$T_r = (T / T_{CT})$	1.50	1.50	1.50					
15	Z (Table XI)	0.783	0.784	0.784					

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FROM KNOWN BOTTOM HOLE PRESSURE (P_f or P_s)

COMPANY Conoco, Inc. LEASE B Section 12 Township 20 S Range 37 E DATE 12-18-84

LOCATION: Unit B L/H 6999' G 0.7573 % CO₂ 0.307 % N₂ 3.488 % H₂S 0.000

GH 5300 P_{cr} 663.7 T_{cr} 369.2

TABLE IX & X

LINE	1	2	3	4	5	6	7	8
1	519	519	520	520	522	522	525	525
2	600	600	600	600	600	600	600	600
3	560	560	560	560	561	561	563	563
4	0.788	0.798	0.791	0.802	0.801	0.813	0.817	0.830
5	441	447	443	449	449	456	460	467
6	12.018	11.857	11.964	11.804	11.804	11.623	11.522	11.349
7	1.569	1.560	1.566	1.557	1.557	1.546	1.540	1.530
8	1962.2	1962.2	1882.2	1882.2	1706.2	1706.2	1486.2	1486.2
9	3850.2	3850.2	3542.7	3542.7	2911.1	2911.1	2208.8	2208.8
10	2453.9	2468.1	2262.3	2275.3	1869.7	1883.0	1434.3	1443.7
11	1566	1571	1504	1508	1367	1372	1198	1202
12	1764.1	1766.6	1693.1	1695.1	1536.6	1539.1	1342.1	1344.1
13	2.66	2.66	2.55	2.55	2.32	2.32	2.02	2.03
14	1.52	1.52	1.52	1.52	1.52	1.52	1.52	1.52
15	0.798	0.798	0.802	0.802	0.813	0.813	0.830	0.830

1st

2nd

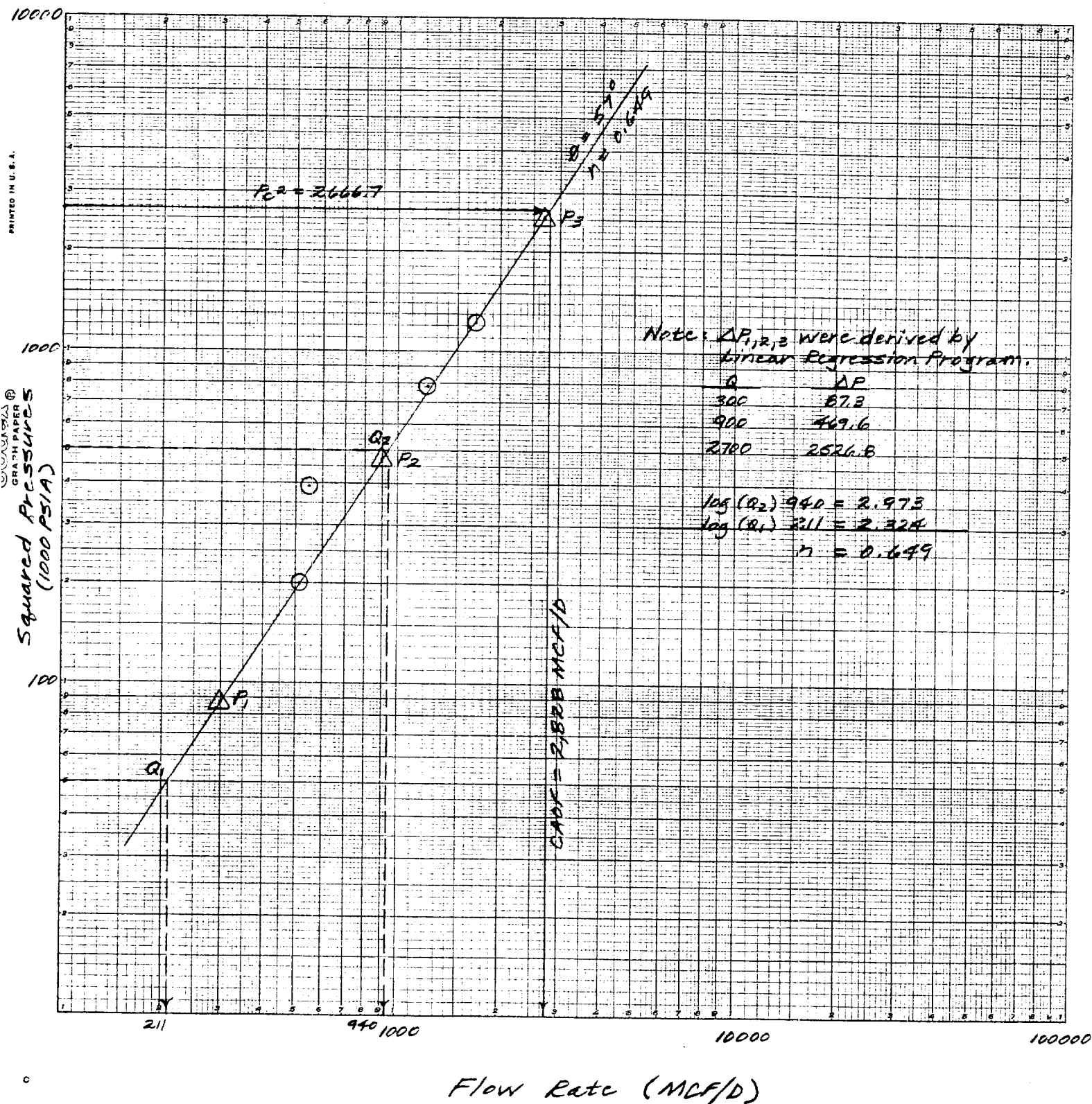
3rd

4th

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