

Submit in duplicate to
appropriate district office
See Rule 401 & Rule 1122

Energy, Minerals and Natural Resources Department

Form C-122
Revised 4-1-91

OIL CONSERVATION DIVISION

P.O. Box 2088
Santa Fe, New Mexico 87504-2088

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator TEXACO EXPLORATION AND PRODUCTION INC.						Lease or Unit Name N.M. H STATE NCT -3					
Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 10-4 to 10-5		Well No. 35			
Completion Date 10-5-94		Total Depth 3565		Plug Back TD 3536		Elevation 3524		Unit Ltr. - Sec. - TWP - Rge. E 19-20S-37E			
Csg. Size 5 1/2	Wt. 15.5	d 4.950	Set At 3565	Perforations: From: 3313 To: 3467				County Lea			
Tbg. Size 2-3/8	Wt. 4.7	d 1.995	Set At 3304	Perforations: From: To:				Pool 			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple single						Packer Set At none		Formation EUMONT VATES 7 RIVE			
Producing Thru TBG.		Reservoir Temp. °F 93		Mean Annual Temp. °F 60		Baro. Press - P _a 13.2		Connection pipeline			
L 3390	H 3390	G _g .734	% CO ₂ 4.31	% N ₂ 1.81	% H ₂ S	Prover		Meter Run		Taps flg.	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							124				
1.							53				24 hrs.
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	COEFFICIENT (24 HOUR)		Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.							
2.							382
3.							
4.							
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl
1.					DRY	
2.					A.P. I. Gravity of Liquid Hydrocarbons DRY	Deg.
3.					Specific Gravity Separator Gas	XXXXXXXXXX
4.					Specific Gravity Flowing Fluid DRY	XXXXXX
5.					Critical Pressure 684 P.S.I.A.	P.S.I.A.
					Critical Temperature 391 R	R

P_c 137.2 P_c² 18.8

NO.	P _i ²	P _w	P _w ²	P _c ² - P _w ²
1.	4.4	80.6	6.5	12.3
2.				
3.				
4.				
5.				

1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.527$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^a = 583$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^a = 1.527$

Absolute Open Flow	583	Mcf/d @ 15.025	Angle of Slope θ	45	Slope, n	1.000
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Remarks:

Approved By Division

Conducted By:
PRO WELL TESTERS

Calculated By:
KS

Checked By:
BM

ON 10-11-94 BY JERRY SEXTON
SUPERVISOR

DEC 8 1994