

NEW MEXICO OIL CONSERVATION COMMISSION  
HOBBS OFFICE OCC

Form C-122

MULTI-POINT BACK PRESSURE TEST FOR GAS IN WELLS 32

Revised 12-1-55

Pool Exmont Formation S.R.-Q County Lea  
Initial \_\_\_\_\_ Annual \_\_\_\_\_ Special X Date of Test 9-21-56  
Company Amerada Petroleum Corporation Lease H.L. Houston Well No. 3  
Unit B Sec. 7 Twp. 21-S Rge. 36-E Purchaser Permian Basin Pipeline  
Casing 6-5/8" Wt. 20.0# I.D. 6.049" Set at 3795' Perf. 3108' To 3648'  
Tubing 2-7/8" Wt. 6.5 I.D. 2.441 Set at 3644' Perf. 3642' To 3644'  
Gas Pay: From 3108' To 3648' L 3642' xG 0.675 -GL 2458 Bar.Press. 13.2  
Producing Thru: Casing \_\_\_\_\_ Tubing X Type Well Single  
Date of Completion: 6-9-54 Packer 3665' Single-Bradenhead-G. G. or G.O. Dual  
Reservoir Temp. \_\_\_\_\_

OBSERVED DATA

Tested Through XXXXXXXXXX (Meter)

Type Taps Pipe

No.	Flow Data					Tubing Data		Casing Data		Duration of Flow Hr.
	(Prover) (Line) Size	(Choke) (Orifice) Size	Press. psig	Diff. h <sub>w</sub>	Temp. °F.	Press. psig	Temp. °F.	Press. psig	Temp. °F.	
SI										
1.	4"	2.25"	473.7	4.5	60			912.4		71.75
2.	4"	2.25"	471.9	8.5	60			883.1		24
3.	4"	2.25"	475.0	14.8	63			845.2		24
4.	4"	2.25"	467.5	20.5	65			790.0		24
5.								724.5		24

FLOW CALCULATIONS

No.	Coefficient (24-Hour)	$\sqrt{h_w p_f}$	Pressure psia	Flow Temp. Factor F <sub>t</sub>	Gravity Factor F <sub>g</sub>	Compress. Factor F <sub>pv</sub>	Rate of Flow Q-MCFPD @ 15.025 psia
1.	40.53	46.81	486.9	0.9813	0.9427	1.042	1829
2.	40.53	64.21	485.1	1.0000	"	1.048	2571
3.	40.53	85.00	488.2	0.9971	"	1.048	3394
4.	40.53	99.27	480.7	0.9952	"	1.046	3949
5.							

PRESSURE CALCULATIONS

Gas Liquid Hydrocarbon Ratio \_\_\_\_\_ cf/bbl.  
Gravity of Liquid Hydrocarbons \_\_\_\_\_ deg.  
F<sub>c</sub> 5.866 (1-e<sup>-s</sup>) 0.156

Specific Gravity Separator Gas \_\_\_\_\_  
Specific Gravity Flowing Fluid \_\_\_\_\_  
P<sub>c</sub> 925.6 P<sub>c</sub><sup>2</sup> 856.7

CO<sub>2</sub> - 1.10% N<sub>2</sub> - 1.30%

No.	P <sub>w</sub> P <sub>t</sub> (psia)	P <sub>c</sub> <sup>2</sup> P <sub>t</sub>	F <sub>c</sub> Q	(F <sub>c</sub> Q) <sup>2</sup>	(F <sub>c</sub> Q) <sup>2</sup> (1-e <sup>-s</sup> )	P <sub>w</sub> <sup>2</sup>	P <sub>c</sub> <sup>2</sup> -P <sub>w</sub> <sup>2</sup>	Cal. P <sub>w</sub>	P <sub>w</sub> P <sub>c</sub>
1.	896.3	803.4	10.73	115.1	17.96	821.36	35.34	906	.98
2.	858.4	736.9	15.08	227.4	35.47	772.37	84.33	880	.95
3.	803.2	645.1	19.91	396.4	61.84	706.94	149.76	840	.91
4.	737.7	544.2	23.17	536.9	83.76	627.96	228.74	791	.85
5.									

Absolute Potential: 9,000 MCFPD; n 0.5 (Assumed)

COMPANY Amerada Petroleum Corporation  
ADDRESS Drawer D - Monument, New Mexico  
AGENT and TITLE W.G. Abbott - District Engineer  
WITNESSED R.L. West  
COMPANY Permian Basin Pipeline Co.

REMARKS

The slope was under 0.5 so a line with a slope of 0.5 was drawn through the lowest flow rate, in accordance with the rules and regulation.

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T.S.A. U.I.  
OCC HOBBS

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

$Q$  = Actual rate of flow at end of flow period at W. H. working pressure ( $P_w$ ).  
MCF/da. @ 15.025 psia and 60° F.

$P_c$  = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater.  
psia

$P_w$  = Static wellhead working pressure as determined at the end of flow period.  
(Casing if flowing thru tubing, tubing if flowing thru casing.) psia

$P_t$  = Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia

$P_f$  = Meter pressure, psia.

$h_w$  = Differential meter pressure, inches water.

$F_g$  = Gravity correction factor.

$F_t$  = Flowing temperature correction factor.

$F_{pv}$  = Supercompressability factor.

$n$  = Slope of back pressure curve.

Note: If  $P_w$  cannot be taken because of manner of completion or condition of well, then  $P_w$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_t$ .