

NEW MEXICO OIL CONSERVATION COMMISSION

MOBDS OFFICE 900 FORM C-122

MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS
Revised 12-1-55

Pool Bumont Formation Green County Lea
Initial Annual Special X Date of Test 6-9/6-13, 1958
Company Shell Oil Company Lease Devonian State Well No. 1
Unit 0 Sec. 20 Twp. 218 Rge. 36S Purchaser El Paso Natural Gas Company
Casing 7 Wt. 23 I.D. 6.336 Set at 3830 Perf. 3060 To 3620
Tubing 2 1/2 Wt. 6.5 I.D. 2.441 Set at 3904 Perf. To
Gas Pay: From 3060 To 3620 L 3060 xG .655 -GL 2004 Bar.Press. 13.2
Producing Thru: Casing X Tubing Type Well G.O. Dual *
Date of Completion: 9-2-53 Packer 3710 Single-Bradenhead-G. G. or G.O. Dual
Reservoir Temp.

OBSERVED DATA *Oil zone temporarily abandoned.

Tested Through (~~PISTON~~) (~~ORIFICE~~) (Meter) Type Taps Flgs.

Flow Data						Tubing Data		Casing Data		Duration of Flow Hr.
No.	(PISTON) (Line) Size	(ORIFICE) (Orifice) Size	Press. psig	Diff. h _w	Temp. °F.	Press. psig	Temp. °F.	Press. psig	Temp. °F.	
SI								<u>946/943/946</u>		<u>24/48/72</u>
1.	<u>4"</u>	<u>1.750</u>	<u>555</u>	<u>10.84</u>	<u>76</u>			<u>878</u>		<u>3</u>
2.	<u>4"</u>	<u>1.750</u>	<u>554</u>	<u>21.16</u>	<u>72</u>			<u>850</u>		<u>3</u>
3.	<u>4"</u>	<u>1.750</u>	<u>551</u>	<u>31.36</u>	<u>70</u>			<u>826</u>		<u>3</u>
4.	<u>4"</u>	<u>1.750</u>	<u>539</u>	<u>43.56</u>	<u>68</u>			<u>804</u>		<u>24</u>
5.										

FLOW CALCULATIONS

No.	Coefficient (24-Hour)	$\sqrt{h_{wpf}}$	Pressure psia	Flow Temp. Factor F _t	Gravity Factor F _g	Compress. Factor F _{pv}	Rate of Flow Q-MCFPD @ 15.025 psia
1.	<u>19.27</u>	<u>76.27</u>	<u>568.2</u>	<u>0.9890</u>	<u>0.9571</u>	<u>1.056</u>	<u>1464</u>
2.	<u>19.27</u>	<u>109.54</u>	<u>567.2</u>	<u>0.9887</u>	<u>0.9571</u>	<u>1.057</u>	<u>2111</u>
3.	<u>19.27</u>	<u>132.99</u>	<u>564.2</u>	<u>0.9905</u>	<u>0.9571</u>	<u>1.057</u>	<u>2569</u>
4.	<u>19.27</u>	<u>155.07</u>	<u>552.2</u>	<u>0.9924</u>	<u>0.9571</u>	<u>1.055</u>	<u>2994</u>
5.							

PRESSURE CALCULATIONS

Gas Liquid Hydrocarbon Ratio dry cf/bbl.
Gravity of Liquid Hydrocarbons deg.
F_c .865 (1-e^{-s}) 0.129

Specific Gravity Separator Gas .655
Specific Gravity Flowing Fluid
P_c 961.2 P_c² 923.9

No.	P _w P _t (psia)	P _t ²	F _c Q	(F _c Q) ²	(F _c Q) ² (1-e ^{-s})	P _w ²	P _c ² -P _w ²	Cal. P _w	P _w P _c
1.	<u>892.2</u>	<u>794.2</u>	<u>1.27</u>	<u>1.61</u>	<u>0.21</u>	<u>794.4</u>	<u>129.5</u>	<u>891.3</u>	<u>92.7</u>
2.	<u>863.2</u>	<u>745.1</u>	<u>1.83</u>	<u>3.35</u>	<u>0.43</u>	<u>745.9</u>	<u>175.4</u>	<u>863.4</u>	<u>89.8</u>
3.	<u>839.2</u>	<u>704.3</u>	<u>2.22</u>	<u>4.93</u>	<u>0.64</u>	<u>704.9</u>	<u>219.0</u>	<u>839.6</u>	<u>87.3</u>
4.	<u>817.2</u>	<u>667.8</u>	<u>2.59</u>	<u>6.71</u>	<u>0.87</u>	<u>668.7</u>	<u>255.2</u>	<u>817.7</u>	<u>85.1</u>
5.									

Absolute Potential: 11,000 MCFPD; n .97
COMPANY Shell Oil Company
ADDRESS Box 845, Roswell, New Mexico
AGENT and TITLE A. L. KILPATRICK - Gas Tester
WITNESSED H. A. KILPATRICK
COMPANY El Paso Natural Gas Company

REMARKS

ILLEGIBLE

INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

NOMENCLATURE

Q = Actual rate of flow at end of flow period at W. H. working pressure (P_w).
MCF/da. @ 15.025 psia and 60° F.

P_c = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater.
psia

P_w = Static wellhead working pressure as determined at the end of flow period.
(Casing if flowing thru tubing, tubing if flowing thru casing.) psia

P_t = Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia

P_f = Meter pressure, psia.

h_w = Differential meter pressure, inches water.

F_g = Gravity correction factor.

F_t = Flowing temperature correction factor.

F_{pv} = Supercompressibility factor.

n = Slope of back pressure curve.

Note: If P_w cannot be taken because of manner of completion or condition of well, then P_w must be calculated by adding the pressure drop due to friction within the flow string to P_t .