						e e e e e e e e e e e e e e e e e e e			(	39 Form C-122
			wiit	ጥፐ _ ነጋብዊ እነጥ :	DACK DDE	מיים מכווסט	ද්රුණය සං	e meric	tu s	Revised 12-1-55
_	,		HOL	TT-FOTMI	DACK FRE	South 15	of roundar	o METITO		]) Form C-122 Revised 12-1-55
Poc	ol _Jelmat	GAR		_Formatio	n_7 R1v	ers		County	Lea	
Initial Annual			Annual	Special			<del></del>	Date of	Test	9/11/61
Con	npany a =	Tong			_Lease_ 😨	ech-St	ata	We]	Ll No.	2
		_								
										. Co.
Cas	ing J	Wt • 14 1	I.D	Se	et at_ <b>39</b>	10Pe	erf3754		To38	00'
Tub	oing 2 3/8	Wt	I.D	S	et at 38	<b>88:</b> Pe	rf. 1820	Garre	<b>†</b> ₺ 51•	e <b>v</b> e
										ss. 13.2
Pro	ducing Thru	: Casir	rg	Tı	ıbi.ng	Sir	Type We	ell Sing	le G. or G	O. Dual
Dat	e of Complet	ion: 12,	/12/56	Packe	r_ None		Reserve	oir Temp.	11	L
		·			OBSERV	ED DATA				
m	1.1 m	(D	) (a) )	) (m )						
Tested Through (Proces) (Meter) Type Taps Fig.										
			w Data			Tubing	Data	Casing D	ata	
No.	(Line)	(Orific	Pres	Bs. Diff.	Temp.	Press.	Temp.	Press.	Temp.	Duration of Flow
	Size	Size	psi	ig h <sub>w</sub>	°F.	ps <b>i</b> g	°F.	psig	<sup>⊃</sup> F•	Hr.
SI						603		617		72 hours
1. 2.	4**	2.750				569	ļ	590		_3_hours
<u>~•</u> 3.	411	2.750   2.750	17		90	547 519	<del> </del>	587	+	3 hours
4.	411	2.750	20			480		554 535		3 hours
<u>5.                                    </u>	_ ‡"	2.750	- 13	8.00	86	470		526		20 hours
					FLOW CAL	CULATION	S_			
,,	Coeffici	.ent		Pressure	Flow	- 1	Gravity	Compre		Rate of Flow
No.	(24-Hou	r)  /	h <sub>w</sub> p <sub>f</sub>	psia	Fac F		Factor <sup>F</sup> g	Facto F <sub>DV</sub>	I	Q-MCFPD 15.025 psia
1.		V	-WFI	Poza		<u> </u>		<del></del>	\ <u>`</u>	- 24 -
2.	53.05		1.23		9813		<del>-9608</del>	Neg.		<del>-561.7</del>
<u>3</u> .	53.05		7.94		9777		-9608	Neg.		894.0
4.	53.05	19.96		9868			-9608_	Neg.		1,004
<b></b>	<del>53.05</del>		5.05		<del>- 9759</del>		<del>-9608</del>	Neg.		1984
				PR	ESSURE C	ALCUTATI	ONS			
ae T	Liquid Hydro	aanhan D	ntio		cf/bbl.		C	e÷ - 0		-1 0
ravi	ity of Liqui	d Hydroc	arbons	6-2/	61/001.		Speci:	iic Gravi fic Gravi	ty Separ tv Flowi	rator Gas 9608 ing Fluid 8789
c			(l-e <sup>-5</sup>	707 00	<del></del>		Pc_ <b>63</b>	0_2	Pc	7_1
							V- <b>U</b> J	442	- · <del></del>	
Т	$P_{\mathbf{w}}$			<del></del>						1
No.		$P_{\mathbf{t}}^{2}$	$\mathtt{F_{c}^{Q}}$	$(F_cQ)^2$	(F	Q) <sup>2</sup> -e-s)	P <sub>w</sub> 2	$P_c^2 - P_w^2$	Cal	Pw Pc
	Pt (psia)			<del> </del>	(1.	-e <sup>-s</sup> )			Pw	<u> </u>
1. 2.	582.2	<del>_339.</del> 0		<del> </del> -			363.8	33.3	603.	2 95.7
3.	530.0	282 2					360.2	<del>-36.9-</del> -	500.	2 95.2
+•	493.2	243.2					300.5	96.6	548	2 90.0
<u>, , , , , , , , , , , , , , , , , , , </u>	483.2	233.5		11.1			290.7	106.4	539	2 85.6
	olute Potent		1,690	Jight U	MCFPD;	n554	<b></b>			
ADDR	ESS 508		ingon-1	loster B	iil laine	Midle	and. Tex	<u> </u>		
	T and TITLE JESSED	C. E.	Long,	Owner	1.84	N.				
	DA NEW	ago Na		es Co.	Jel M	ew Mexi				
			<del>v qea oldU</del>		REM/	RKS	····			

This test was conducted by J. B. Murray, El Paso Natural Gas Co with C. E. Long as witness.

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

- Q I Actual rate of flow at end of flow period at W. H. working pressure (Pw). MCF/da. @ 15.025 psia and 60° F.
- PcI 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- Pw Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- $P_{f}$  Meter pressure, psia.
- $h_{\mathbf{W}}$  Differential meter pressure, inches water.
- $F_g$ : Gravity correction factor.
- Ft Flowing temperature correction factor.
- Fpv Supercompressability factor.
- n I Slope of back pressure curve.

Note: If  $P_{\mathbf{W}}$  cannot be taken because of manner of completion or condition of well, then  $P_{\mathbf{W}}$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_{\mathbf{t}}$ .