

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122 -
Revised 9-1-65

Type Test ☐ Initial ☐ Annual ☒ Special					Test Date 2-15-90		RECLASSIFICATION TO GAS WELL		
Company SHELL WESTERN E&P INC.					Connection		1-PT TEST		
Pool NORTH EUNICE BLINEBRY-TUBB- DRINKARD OIL & GAS					Formation BLINEBRY		Unit NORTHEAST DRINKARD		
Completion Date 12-05-89		Total Depth 6723'		Plug Back TD 6125'		Elevation 3448' DF		Farm or Lease Name	
Cs. Size 5-1/2"	Wt. 14, 17#	d 4.95"	Set At 6722'	Perforations: From 5584' To 5670'		Well No. 405			
Thq. Size 2-7/8"	Wt. 6.5	d 2.441"	Set At 5705'	Perforations: From To		Unit B	Sec. 10	Twp. 21S	Rge. 37E
Type Well - Single - Broadhead - G.G. or G.O. Multiple					Packer Set At -----		County LEA		
Producing Thru TBG		Reservoir Temp. °F 151 @ 5627'		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2		State NM	
L 6320	H ----	G _g .777	% CO ₂ .092	% N ₂ 1.83	% H ₂ S TR	Prover BARTON	Meter Run 2.067	Taps FLG	

FLOW DATA							TUBING DATA		CASING DATA		Duration
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	of Flow
SI	4 WEEKS						143	44			
1.	2.067 X 0.500			41.0	22	42	41	42			24 HRS
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	1.189	34.53	54.2	1.018	1.134	1.011	48
2							
3							
4							
5							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.			
1.	.08	611	1.49	.979	A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.			
2.					Specific Gravity Separator Gas _____ XXXXXXXXXX			
3.					Specific Gravity Flowing Fluid _____ XXXXX			
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.			
5.					Critical Temperature _____ R _____ R			

P _c 156.2 P _c ² 24.4				
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²
1	2.938	1.72	2.96	21.44
2				
3				
4				
5				

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 1.138$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 54.6$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.138$$

Absolute Open Flow	54.6 Mcfd @ 15.025	Angle of Slope θ	45°	Slope, n	1.000
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Remarks: DID NOT ATTEMPT 4-PT TEST DUE TO LOW DAILY FLOW.
WELL REMAINS SHUT-IN.

MAR 14 1990

Approved By Commission:
SIGNED BY JERRY SEXTON
DISTRICT 1 SUPERVISOR

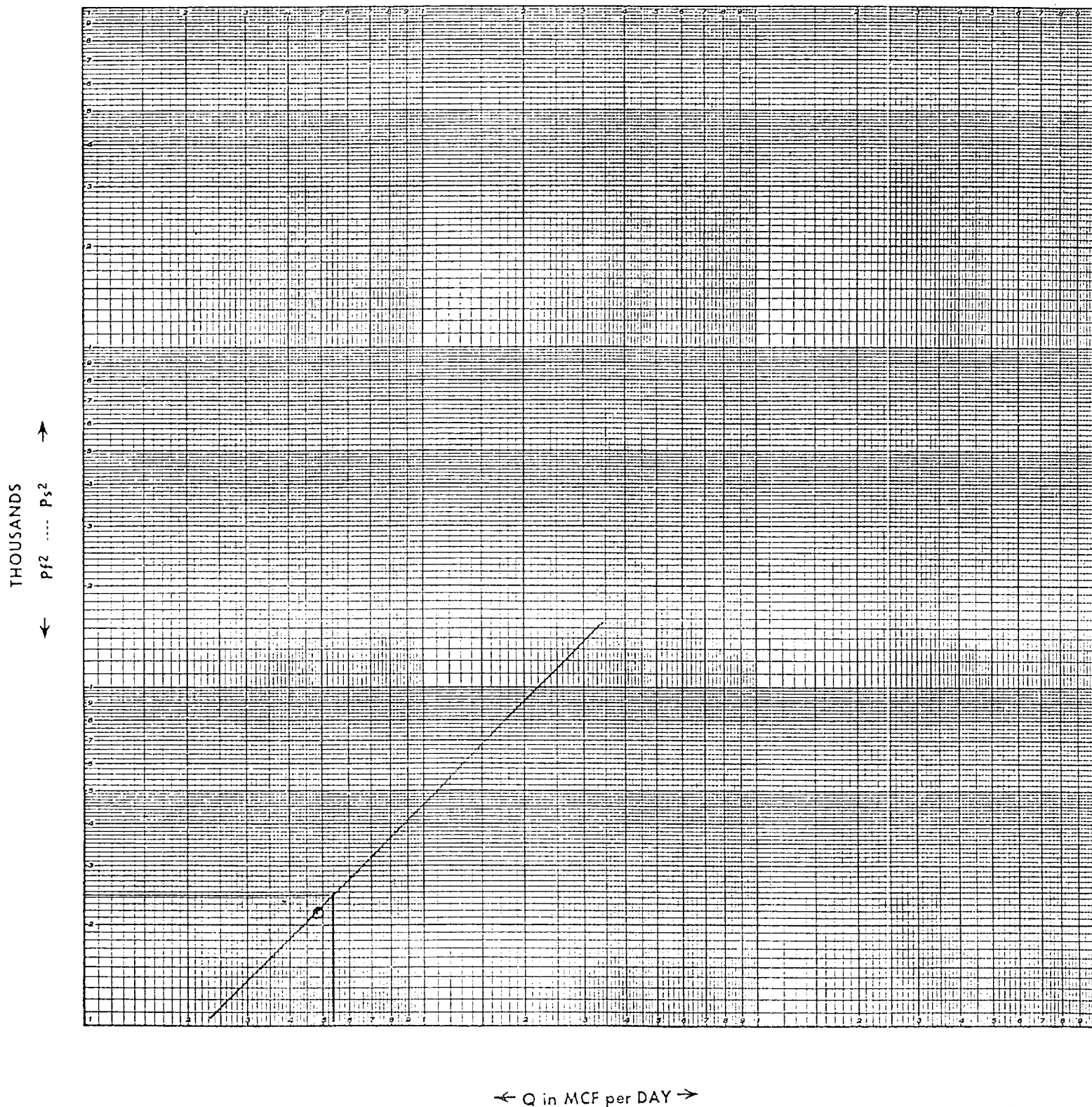
Conducted By:
D. E. ASHMORE

Calculated By:
D. E. ASHMORE

Checked By:

GAS WELL
BACK PRESSURE CURVE

County Lea Field DRINKARD
Operator Shell Western E&P Inc
Lease N.E.D.U. Well No. 405
Volume 54.6 MCF/24 hr.
Date 2-15-90



WORKSHEET FOR CALCULATION OF STAINLESS COLUMN WELLHEAD PRESSURE (P_w)

COMPANY Shell Western E&P LEASE N.E. 1/4, 22, 14N, 24E WELL NO. 405 DATE 2-15-93

LOCATION: Unit B Section 10 Township 21S Range 37E

L	6320'	H	-	L/H	632.0	G	1.777	%CO ₂	0.92	%N ₂	1.83	%H ₂ S	Tr.
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RECEIVED

MAR 12 1999

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HOBBS OFFICE