

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test ☐ Initial ☐ Annual ☒ Special						Test Date 5-11-89		RECLASSIFICATION TO	
Company SHELL WESTERN E&P INC.				Connection ENRON				GAS WELL	
Pool BLINEBRY (PRO GAS) (CONSOL.)				Formation BLINEBRY				Unit NORTHEAST DRINKARD	
Completion Date 3-29-89		Total Depth 7503'		Plug Back TD 5685'		Elevation 3411' GR		Farm or Lease Name	
Csj. Size 5-1/2"	Wt. 17#	d 4.95"	Set At 7465'	Perforations: From 5526 To 5627		Well No. 710			
Tbg. Size 2-3/8"	Wt. 4.70	d 1.995	Set At 5471'	Perforations: From To		Unit P	Sec. 15	Twp. 21S	Rge. 37E
Type Well - Single - Bradenhead - G.G. or G.O. Multiple				Packer Set At 5453'		County LEA			
Producing Thru TBG		Reservoir Temp. °F 151° @ 5577'		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2		State NM	
L 5471	H 5471	G _g .688	% CO ₂ .04	% N ₂ 2.05	% H ₂ S 0%	ORIFICE METER	Meter Run 2.066	Taps FLG	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI	2.066		0.500	72 HRS			220	55			72 HRS
1.	2.066		0.500	46	44	74	194	63			5 HRS
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	1.189	51.04	59.2	.9868	1.206	1.059	77
2							
3							
4							
5							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1.	0.088	534	1.41	.891	A.P.I. Gravity of Liquid Hydrocarbons	Deq.
2.					Specific Gravity Separator Gas	.688
3.					Specific Gravity Flowing Fluid	XXXXXX
4.					Critical Pressure	672 P.S.I.A.
5.					Critical Temperature	379 °R

P _c 233.2 P _c ² 54.4				
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²
1	42.9		43.0	11.4
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 4.772$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 4.772$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 367$

Absolute Open Flow 367 Mcfd @ 15.025	Angle of Slope θ 45°	Slope, n 1.000
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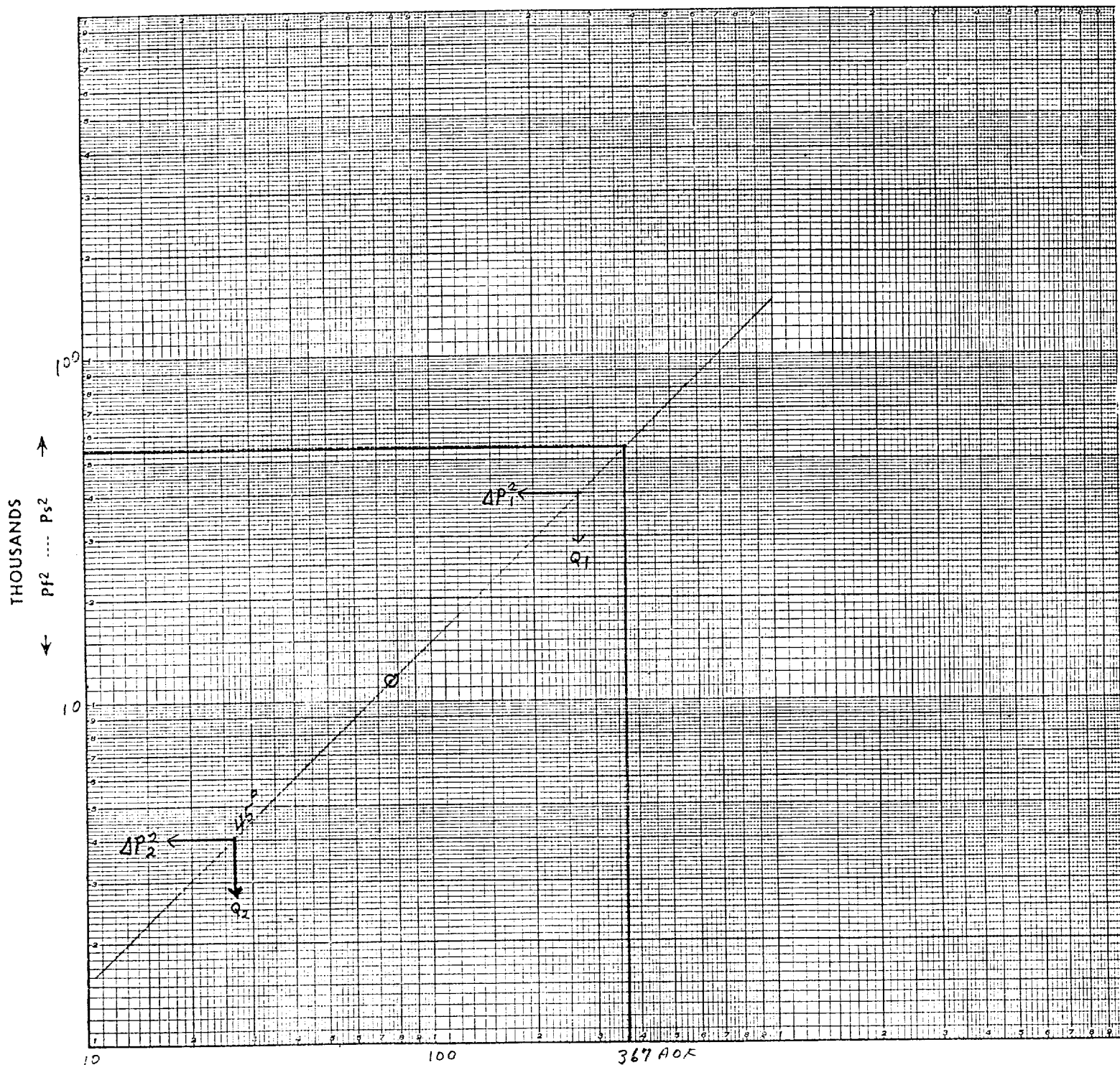
Remarks: DID NOT ATTEMPT 4-PT TEST DUE TO LOW DAILY FLOW.

JUN 21 1989

ORIGINAL SIGNED BY JERRY SEXTON District Supervisor	Conducted By: D. E. ASHMORE	Calculated By: D. E. ASHMORE	Checked By:
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**GAS WELL
BACK PRESSURE CURVE**

County Le2 Field N.E.D.U.
 Operator Shell Western E & P
 Lease Well No. 710
 Volume MCF/24 hr.
 Date 5-11-89



$$\Delta P_1^2 \quad P_c^2 - P_w^2 = 400$$

$$\Delta P_2^2 \quad P_c^2 - P_w^2 = 40$$

$$Q_1 = 270 \text{ MCFD}$$

$$Q_2 = 27 \text{ MCFD}$$

← Q in MCF per DAY →

$$\log Q_1 = 2.431$$

$$\log Q_2 = 1.431$$

$$n = 1.000$$

WORKSHEET FOR CALCULATION OF STAINLESS COLUMN WELLHEAD PRESSURE (P_w)

COMPANY

Shell Western Exp LEASE

N: E: D: U:

WELL NO. 1

710

1

DATE:

11-89

LOCATION: Unit 11 P

2

Section _____

15

Township.

215

Range.

37 E

1

L 5471 H

547

L/H

000

889

 CO_2 —

4 %

2.05

% H₂S

0

—p

1.995

F I

231

3764

F

672
TABLE IX B X

Tcr -

19
—
X X X X

[illegible]