

## NEW MEXICO OIL CONSERVATION COMMISSION

Form C-122

## MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Revised 12-1-55

Pool Tubb (Gas) Formation Tubb County Lea State N.M.  
Initial X Annual \_\_\_\_\_ Special \_\_\_\_\_ Date of Test 6-13-58  
Company Tidewater Oil Company Lease Percy Hardy Well No. 2  
Unit 0 Sec. 17 Twp. 21S Rge. 37E Purchaser El Paso Natural Gas Co.  
Casing 5-2/8" Wt. 15.5 I.D. 4.950 Set at 6650 Perf. 6200 To 6300  
Tubing 2-3/8" Wt. 4.7 I.D. 1.995 Set at \_\_\_\_\_ Perf. \_\_\_\_\_ To \_\_\_\_\_  
Gas Pay: From 6200 To 6300 L. 6240 xG .695 -GL 4336.8 Bar.Press. 13.2  
Producing Thru: Casing X Tubing \_\_\_\_\_ Type Well G.O. Dual  
Date of Completion: 12-18-57 Packer 6540 ✓ Single-Bradenhead-G. G. or G.O. Dual  
Reservoir Temp. Unknown

## OBSERVED DATA

Tested Through (Prover) (Choke) (Meter) Type Taps Flange

No.	Flow Data					Tubing Data		Casing Data		Duration of Flow Hr.
	(Prover) (Line) Size	(Choke) (Orifice) Size	Press. psig	Diff. h <sub>w</sub>	Temp. °F.	Press. psig	Temp. °F.	Press. psig	Temp. °F.	
SI								1131		
1.	4	.750	4.65	2.3	66			1030		3
2.	4	.750	5.0	3.6	65			891		3
3.	4	.750	4.85	6.0	64			621		3
4.	4	.750	4.6	7.4	71			335		3
5.	4	.750	4.5	6.0	70			225		24

## FLOW CALCULATIONS

No.	Coefficient (24-Hour)	$\sqrt{h_w p_f}$	Pressure psia	Flow Temp. Factor F <sub>t</sub>	Gravity Factor F <sub>g</sub>	Compress. Factor F <sub>pv</sub>	Rate of Flow Q-MCFPD @ 15.025 psia
1.	10.8615	10.695	216.2	0.9943	.9292	1.022	109.68
2.	10.8615	18.000	250	0.9952	.9292	1.029	186.03
3.	10.8615	29.10	235.2	0.9962	.9292	1.027	300.48
4.	10.8615	34.04	211.6	0.9896	.9292	1.023	347.78
5.	10.8615	27.00	202.5	0.9850	.9292	1.023	274.32

## PRESSURE CALCULATIONS

Gas Liquid Hydrocarbon Ratio \_\_\_\_\_ cf/bbl.  
Gravity of Liquid Hydrocarbons \_\_\_\_\_ deg.  
F<sub>c</sub> .9274 (1-e<sup>-S</sup>) .258

Specific Gravity Separator Gas .695  
Specific Gravity Flowing Fluid 1.14  
P<sub>c</sub> 1131 P<sub>c</sub> 1,279,161

No.	P <sub>t</sub> (psia)	P <sub>t</sub> <sup>2</sup>	F <sub>c</sub> Q	(F <sub>c</sub> Q) <sup>2</sup>	(F <sub>c</sub> Q) <sup>2</sup> (1-e <sup>-S</sup> )	P <sub>w</sub> <sup>2</sup>	P <sub>c</sub> <sup>2</sup> -P <sub>w</sub> <sup>2</sup>	Cal. P <sub>w</sub>	P <sub>w</sub> /P <sub>c</sub>
1.	1030	1,060,900	.101717	.01035	.00267	1060.903	218,248	1030.1	.9108
2.	891	793,881	.172424	.02976	.00768	793.889	485,272	891.1	.7879
3.	621	385,641	.278665	.07765	.02003	385.661	893,500	621.1	.5492
4.	335	112,225	.322531	.10403	.02684	112,232	1,166,910	335.1	.2963
5.	225	50,625	.2584	.06672	.01670	50,792	1,228,369	225.1	.19903

Absolute Potential: 300 MCFPD; n .672

COMPANY Tidewater Oil Company  
ADDRESS Box 547 Hobbs, New Mexico  
AGENT and TITLE Grady Oden, Gas Tester  
WITNESSED John Springer  
COMPANY Tidewater Oil Company

REMARKS

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

- $Q$  = Actual rate of flow at end of flow period at W. H. working pressure ( $P_w$ ).  
MCF/da. @ 15.025 psia and 60° F.
- $P_c$  = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater.  
psia
- $P_w$  = Static wellhead working pressure as determined at the end of flow period.  
(Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- $P_t$  = Flowing wellhead pressure (tubing if flowing through tubing, casing if  
flowing through casing.) psia
- $P_f$  = Meter pressure, psia.
- $h_w$  = Differential meter pressure, inches water.
- $F_g$  = Gravity correction factor.
- $F_t$  = Flowing temperature correction factor.
- $F_{pv}$  = Supercompressability factor.
- $n$  = Slope of back pressure curve.

Note: If  $P_w$  cannot be taken because of manner of completion or condition of well, then  $P_w$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_t$ .