

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND E POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 4-9-72				
Company Schlumberger Petroleum Co.				Connection NONE					
Pool Undesignated				Formation San Andres				Unit 120	
Completion Date 3-31-72		Total Depth 11146'		Plug Back TD 1271'		Elevation 3500' KB		Farm or Lease Name Advent A	
Csg. Size 8 1/2"	Wt. 7.0	d. 4.892	Set At 1112'	Perforations: From 1096' To 1120'				Well No. 2	
Tbg. Size 8 3/8"	Wt. 4.7	d. 4.095	Set At 3838'	Perforations: From OPEN To ENDED				Unit Sec. Twp. Rge. 11 6 21 37	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE				Packer Set At 3848' KB				County Tola	
Producing Thru Tubing		Reservoir Temp. °F 128 @ 3800'		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2		State New Mexico	
L 1113	H -	Gg 0.661	% CO ₂ 5.11	% N ₂ 0.25	% H ₂ S 0.00	Prover		Meter Run Y	Taps 7

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g. DWT	Temp. °F	Press. p.s.i.g.	
SI	1		2				1221		PACKED	
1.	1	11/64	2	580	54	74	807	77		
2.	1	33/64	2	580	46	74	894	77		
3.	1	25/64	2	580	32	73	985	78		
4.	1	20/64	2	580	17	75	1045	78		
5.										

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	19.81	175.97	593.2	0.9868	1.227	1.019	1503.1
2	15.81	165.12	593.2	0.9868	1.227	1.019	1156.1
3	10.81	139.78	593.2	0.9877	1.227	1.050	747.0
4	10.81	106.17	593.2	0.9859	1.227	1.019	3525.6
5.							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1	0.85	534	1.17	0.909	9.007	
2.	0.85	534	1.17	0.909	A.P.I. Gravity of Liquid Hydrocarbons	Deg.
3.	0.85	534	1.17	0.909	Specific Gravity Separator Gas	XXXXXXX
4.	0.85	534	1.17	0.909	Specific Gravity Flowing Fluid	XXXXX
5.					Critical Pressure	P.S.I.A.
					Critical Temperature	R

NO.	P _t ²	P _w ²	R _w ²	P _c ² - R _w ²	$(1) \frac{P_c^2}{P_c^2 - R_w^2} = 5.318$ $(2) \left[\frac{P_c^2}{P_c^2 - R_w^2} \right]^n = 3.055$ $AOF = Q \left[\frac{P_c^2}{P_c^2 - R_w^2} \right]^n = 13757$
1	-	1212.0	1558.0	360.0	
2	-	1241.2	1508.0	320.6	
3	-	1201.0	1475.0	213.0	
4	-	1206.0	1466.0	152.0	

Absolute Open Flow		Mcf @ 15.025		Angle of Slope @ 56° 18'		Slope, n 0.665	
Remarks: * SHF @ (-410') 1113' used for pressure calculations							
Approved By Commission:		Conducted By:		Calculated By:		Checked By:	
		COLMAN P.T. ENG. CO.		JOE A. COLMAN		JOE A. COLMAN	

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OIL CONSERVATION COMM.
HOODS, N. H.