

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 2-6-80				
Company BELCO PETROLEUM CORPORATION				Connection PHILLIPS PETROLEUM COMPANY					
Pool Undesignated - Wilson Penn				Formation STRAWN - <i>or JWR</i>				Unit	
Completion Date 2-6-80		Total Depth 12,797		Plug Back TD 11,460		Elevation 3805 GL		Farm or Lease Name STATE 12	
Csg. Size 7"	Wt. 32.00	d 6.094	Set At 11,455	Perforations: From 11,323 To 11,420		Well No. 1			
Tbg. Size 2 7/8"	Wt. 6,500	d 3.093	Set At 11,198	Perforations: From OPEN To END		Unit Sec. Twp. Rge. G 12 21S 34E			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE				Packer Set At 10,973		County LEA			
Producing Thru TUBING		Reservoir Temp. °F 187° @ 11,372		Mean Annual Temp. °F		Baro. Press. - P _a 13.2		State NEW MEXICO	
L 11,372	H 11,372	G _g .695	% CO ₂ .243	% N ₂ 1.34	% H ₂ S	Prover	Meter Run 2"	Taps FLG	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							1183				
1.	2 x 1.00			30	3	62°	35				
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	4,946	11.38	43.2	.9981	1.200	NIL	67
2.							
3.							
4.							
5.							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio 17.632 Mcf/bbl.	
1.	.06	522	1.35	NIL	A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.	
2.					Specific Gravity Separator Gas .695 XXXXXXXXXX	
3.					Specific Gravity Flowing Fluid XXXXXX	
4.					Critical Pressure 669 P.S.I.A. _____ P.S.I.A.	
5.					Critical Temperature 388 R _____ R	

P _c 1583.1	P _c ² 2506.2		
NO.	P _w ²	P _w	P _c ² - P _w ²
1	776.5	603.0	1903.2
2			
3			
4			
5			

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.317$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.317$

AOP = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = .882$

Absolute Open Flow 882 Mcfd @ 15.025	Angle of Slope θ 45	Slope, n 1.00
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Remarks: WELL MADE 3.8 BBLs. OF CONDENSATE DURING TEST. BOTTOM HOLE PRESSURES MEASURES WITH KUSTER GAUGE.

Approved By Commission: <i>John W. Ryan</i>	Conducted By: W.S.	Calculated By: R.R.	Checked By: J.W.W.
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OIL CONSERVATION DIV.

FEB 18 '80

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