

W MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

☒ Initial ☐ Annual ☐ Special 6/4/81			
Company Getty Oil Company		Connection flare (unconnected)	
Well Wildcat		Location Morrow	
Completion Date 7/27/81	Total Depth 14523	Plug Back TD 14440	Well Head 3636.5
Name of Lease Owner North Bilbrey "18" Fed			
Csg. Size 4 1/2	Wt. 13.5	Set At 14523	Perforations: From 14048 To 14072
Trg. Size 2 3/8	Wt. 4.7#	d 1.995	Perforations: From To
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single		Packer Set At 13690' (wireline depth)	County Lea
Producing Thru Tubing	Reservoir Temp. °F 198°@14523	Mean Annual Temp. °F 60° F	Baro. Press. - P _a 13.2
L 13690	H 13690	G _g 0.6200	% CO ₂ 1.076
		% N ₂ .344	% H ₂ S 0
		Prover 3"	Meter Run 3"
			Tops Flange

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							4725	65	Packer		SI
1.	3"	X	1.5	300	4	76	4525	65			1 hour
2.			1.5	300	7	73	4410	65			1 hour
3.			1.5	300	21	62	4075	65			1 hour
4.			1.5	300	77	50	3020	65			1 hour
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcf/d
1							
2.	11.13	35.39	313.2	.9850	1.2700	1.026	505
3.	11.13	46.82	313.2	.9877	1.2700	1.027	671
4.	11.13	81.00	313.2	.9981	1.2700	1.028	1176
5.	11.13	155.29	313.2	1.010	1.2700	1.032	2288

NO.	R _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.	.464	536	1.48	.950	16.1 Mcf/bbl.	46.7 Deg.			675 P.S.I.A.	363 R
2.	.464	533	1.47	.948			X X X X X X X X			
3.	.464	522	1.44	.947			X X X X X			
4.	.464	510	1.30	.942						
5.										

NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²
1		6108	37308	3345
2		5974	35689	4965
3		5571	31036	9617
4		4346	18888	24766
5				

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 1.641$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3324$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.453$$

Absolute Open Flow 3,324 Mcfd @ 15.025	Angle of Slope θ Slope, n .7537
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Remarks: Bottom hole pressures measured at midpoint of perfs

Approved By Commission: Jerry	Conducted By: Murray & McCurry	Calculated By: Murray	Checked By: Botes
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