

Type Test

☒ Initial

☐ Annual

☐ Special

Test Date

12-15-88

Company

CONOCO, INC

Connection

EPNG PIPELINE

Pool

EUMONT

Formation

QUEEN

Unit

P

Completion Date

10-25-88

Total Depth

3750

Plug Back TD

3740

Elevation

3638 GL

Farm or Lease Name

MEYER B-17

Coq. Size

5.5

Wt.

15.5

d

4.950

Set At

3750

Perforations:

From 3594 To 3680

Well No.

3

Tiq. Size

2.375

Wt.

4.7

d

1.995

Set At

3499

Perforations:

From OPEN To ENDED

Unit

P

Sec.

17

Twp.

215

Ry

36E

Type Well - Single - Bradenhead - G.G. or G.O. Multiple

SINGLE-GAS

Packer Set At

3499

County

LEA

Producing Thru

TUBING

Reservoir Temp. °F

108 @ 3637

Mean Annual Temp. °F

60

Baro. Press. - P<sub>a</sub>

13.2

State

NEW MEXICO

L

3637

H

3637

Cg

.722

% CO<sub>2</sub>

4.57

% N<sub>2</sub>

1.47

% H<sub>2</sub>S

.24

Provor

-

Meter Run

4.0

Taps

FLANGE

FLOW DATA

TUBING DATA

BHP DATA

Duration of Flow

| NO. | Provor Line Size | X | Orifice Size | Press. p.s.i.g. | Diff. h <sub>w</sub> | Temp. °F | Press. p.s.i.g. | CHOKE     | Press. p.s.i.g. | Temp. °F | Duration of Flow |
|-----|------------------|---|--------------|-----------------|----------------------|----------|-----------------|-----------|-----------------|----------|------------------|
| SI  |                  |   |              |                 |                      |          | 215             | -         | 237             | 108      | 24               |
| 1.  | 4.03X1.250       |   |              | 48              | 4.0                  | 36       | 200             | 11 1/2/64 | 223             | 108      | 2                |
| 2.  | 4.03X1.250       |   |              | 47              | 6.8                  | 40       | 193             | 13/64     | 217             | 108      | 1                |
| 3.  | 4.03X1.250       |   |              | 46              | 14.4                 | 41       | 177             | 16 1/2/64 | 205             | 108      | 1                |
| 4.  | 4.03X1.250       |   |              | 46              | 25.0                 | 44       | 161             | 19 1/2/64 | 195             | 108      | 1                |
| 5.  |                  |   |              |                 |                      |          |                 |           |                 |          |                  |

RATE OF FLOW CALCULATIONS

| NO. | Coefficient (24 Hour) | $\sqrt{h_w P_m}$ | Pressure P <sub>m</sub> | Flow Temp. Factor Ft. | Gravity Factor Fg | Super Compress. Factor, Fpv | Rate of Flow Q, Mcfd |
|-----|-----------------------|------------------|-------------------------|-----------------------|-------------------|-----------------------------|----------------------|
| 1   | 7.47                  | 15.62            | 61.0                    | 1.0239                | 1.1769            | 1.0076                      | 142                  |
| 2   | 7.47                  | 20.16            | 60.1                    | 1.0198                | 1.1769            | 1.0073                      | 182                  |
| 3   | 7.47                  | 29.34            | 59.6                    | 1.0188                | 1.1769            | 1.0072                      | 265                  |
| 4   | 7.47                  | 38.54            | 59.4                    | 1.0157                | 1.1769            | 1.0071                      | 347                  |
| 5   |                       |                  |                         |                       |                   |                             |                      |

| NO. | P <sub>t</sub> | Temp. °R | T <sub>r</sub> | Z     | Gas Liquid Hydrocarbon Ratio | A.P.I. Gravity of Liquid Hydrocarbons | Specific Gravity Separator Gas | Specific Gravity Flowing Fluid | Critical Pressure | Critical Temperature |
|-----|----------------|----------|----------------|-------|------------------------------|---------------------------------------|--------------------------------|--------------------------------|-------------------|----------------------|
| 1   | 0.09           | 496      | 1.29           | 0.985 | 0                            | 0                                     | 0.722                          | XXXXXXX                        | 685               | 385                  |
| 2   | 0.09           | 500      | 1.30           | 0.986 |                              |                                       |                                |                                |                   |                      |
| 3   | 0.09           | 501      | 1.30           | 0.986 |                              |                                       |                                |                                |                   |                      |
| 4   | 0.09           | 504      | 1.31           | 0.986 |                              |                                       |                                |                                |                   |                      |
| 5   |                |          |                |       |                              |                                       |                                |                                |                   |                      |

P<sub>c</sub> 227.8

P<sub>c</sub><sup>2</sup> 52

| NO. | P <sub>t</sub> | P <sub>w</sub> | P <sub>w</sub> <sup>2</sup> | P <sub>c</sub> <sup>2</sup> - P <sub>w</sub> <sup>2</sup> |
|-----|----------------|----------------|-----------------------------|-----------------------------------------------------------|
| 1   |                | 215            | 46                          | 6                                                         |
| 2   |                | 209            | 44                          | 8                                                         |
| 3   |                | 199            | 40                          | 12                                                        |
| 4   |                | 189            | 36                          | 16                                                        |
| 5   |                |                |                             |                                                           |

(1)  $\frac{P_c^2}{P_c^2 - P_w^2} = 3.2500$

(2)  $\left[ \frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.944$

AOF = 0

$\left[ \frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1022$

Absolute Open Flow

1022

Mcfd @ 15.025

Angle of Slope @

47.5

Slope, n

0.916

Remarks:

BHP MEASURED WITH AMERADA PRESSURE ELEMENTS

JAN 12 1989

Approved By Division

Conducted By:

Calculated By:

Checked By:

Orig. Signed by

BENNETT CATHEY

MATT LEE

Paul Kautz

Geologist