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appropriate district office
See Rule 401 & Rule 1122

State of New Mexico
Energy, Minerals and Natural Resources Department

Form C-122
Revised 4-1-91

OIL CONSERVATION DIVISION

P.O. Box 2088
Santa Fe, New Mexico 87504-2088

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator MERIDIAN OIL INC.						Lease or Unit Name SHELL STATE COM. d					
Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 1/15/93		Well No. 13			
Completion Date 12/31/92		Total Depth 3600		Plug Back TD 3575		Elevation		Unit Ltr. - Sec. - TWP - Rge. L 36 21S 36E			
Csg. Size 4 1/2"	Wt. 11.6	d	Set At 3600	Perforations: From: 3390 To: 3544				County LEA			
Tbg. Size 2 3/8"	Wt. 4.7	d	Set At 3375	Perforations: From: To:				Pool EUMONT YT-7RVS-QN			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE						Packer Set At NONE		Formation QUEEN			
Producing Thru TBG		Reservoir Temp. °F 108° @ 3375		Mean Annual Temp. °F 60°		Baro. Press - P _a 13.2		Connection VENTED			
L 3375	H 3375	Gg .744	% CO ₂ 9.50	% N ₂ .68	% H ₂ S	Prover 2"	Meter Run		Taps		

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI						269		267		24 HRS.
1.	2	X .625	19.0		58	257		257		1 HR
2.	2	X .625	33.0		59	247		250		1 HR
3.	2	X .625	52.0		61	217		243		1 HR
4.	2	X .625	73.0		64	126		232		1 HR
5.										

RATE OF FLOW CALCULATIONS							
NO.	COEFFICIENT (24 HOUR)	h _w P _m	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg.	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	6.473		32.2	1.002	1.159	1.001	242
2.	6.473		46.2	1.001	1.159	1.001	347
3.	6.473		65.2	.9990	1.159	1.002	490
4.	6.473		86.2	.9962	1.159	1.002	646
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	DRY GAS	Mcf/bbl
1.	.04	518	1.33	.998	A.P.I. Gravity of Liquid Hydrocarbons	DRY	Deg.
2.	.06	519	1.33	.998	Specific Gravity Separator Gas	.744	XXXXXXXXXX
3.	.09	521	1.34	.997	Specific Gravity Flowing Fluid	XXXXXX	
4.	.12	524	1.35	.996	Critical Pressure * 706	P.S.I.A.	P.S.I.A.
5.					Critical Temperature * 388	R	R

P _c 282.2		P _c ² 79.6		1) $\frac{P_c^2}{P_c^2 - P_w^2} = \underline{4.082}$		(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \underline{3.880}$	
NO.	P _i ²	P _w	P _w ²	P _c ² - P _w ²			
1.		270.2	73.0	6.6			
2.		263.2	69.2	10.4			
3.		256.2	65.6	14.0			
4.		245.2	60.1	19.5			
5.							

Absolute Open Flow 2,506 Mcfd @ 15.025		Angle of Slope θ 46°	Slope, n .964
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Remarks: *** CORRECTED TO 9.50% CO2**

NO FLUID PRODUCED DURING TEST

Approved By Division ORIGINAL SIGNED BY JERRY SEXTON	Conducted By: JOHN WEST ENGINEERING	Calculated By: BM	Checked By: BM
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DISTRICT SUPERVISOR