

Submit in duplicate to
appropriate district office
See Rule 401 & Rule 1122

State of New Mexico
Energy, Minerals and Natural Resources Department

Form C-122
Revised 4-1-91

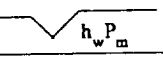
OIL CONSERVATION DIVISION

P.O. Box 2088
Santa Fe, New Mexico 87504-2088

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator MERIDIAN OIL INC						Lease or Unit Name SHELL STATE COM A					
Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 9/20/93		Well No. 6			
Completion Date 9/8/93		Total Depth 3730		Plug Back TD 3660		Elevation		Unit Ltr. - Sec. - TWP - Rge. D 2 21S 36E			
Csg. Size 1 1/2		Wt. 1.6		Set At		Perforations:		County LEA			
Tbg. Size 2 3/8		Wt. 4.7		Set At 1.995		Perforations:		Pool EUMONT			
						From: 3527 To: 3648					
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE						Packer Set At		Formation QUEENS			
Producing Thru TBG		Reservoir Temp. °F		Mean Annual Temp. °F		Baro. Press - P _a 13.2		Connection VENTED			
L	H	Gg .682	% CO ₂ .89	% N ₂ 3.00	% H ₂ S	Prover 2"	Meter Run		Taps FLG		

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							240		238		72 HRS
1.	2	X	.500	5.0		100	190		229		1 HR
2.	2	X	.500	8.0		103	151		228		30 MIN
3.	2	X	.500	10.0		104	130		226		30 MIN
4.	2	X	.500	15.0		104	110		221		30 MIN
5.											

RATE OF FLOW CALCULATIONS							
NO.	COEFFICIENT (24 HOUR)		Pressure P _m	Flow Temp. Factor FL	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	4.279		18.2	.9636	1.211	1.001	91
2.	4.279		21.2	.9610	1.211	1.002	106
3.	4.279		23.2	.9602	1.211	1.002	116
4.	4.279		28.2	.9602	1.211	1.002	141
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	DRY GAS	Mcf/bbl.
1.	.02	560	1.48	.998	A.P. I. Gravity of Liquid Hydrocarbons	DRY	Deg.
2.	.03	563	1.49	.997	Specific Gravity Separator Gas	.682	XXXXXXXXXX
3.	.03	564	1.50	.997	Specific Gravity Flowing Fluid	XXXXXX	
4.	.04	564	1.50	.996	Critical Pressure	* 664	P.S.I.A. P.S.I.A.
5.					Critical Temperature	* 376	R R

P _c <u>253.2</u> P _c ² <u>64.1</u>					1) $\frac{P_c^2}{P_c^2 - P_w^2} = \underline{6.892}$		(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \underline{3.767}$	
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \underline{.531}$			
1.		242.2	58.7	5.4				
2.		241.2	58.2	5.9				
3.		239.2	57.2	6.9				
4.		234.2	54.8	9.3				
5.								

Absolute Open Flow <u>531</u> Mcfd @ 15.025		Angle of Slope θ <u>55.5</u>		Slope, n <u>.687</u>	
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Remarks: NO FLUID PRODUCED DURING TEST. * CORRECTED TO 3.00% N2

Approved By Division	Conducted By: JOHN WEST ENGINEERING	Calculated By: BM	Checked By: BM
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