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See Rule 401 & Rule 1122

State of New Mexico
Energy, Minerals and Natural Resources Department

Form C-122
Revised 4-1-91

OIL CONSERVATION DIVISION

P.O. Box 2088
Santa Fe, New Mexico 87504-2088

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator TEXACO EXPLORATION						Lease or Unit Name SKELLY B STATE COMM					
Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 11-7-94		Well No. 3			
Completion Date		Total Depth 3700		Plug Back TD 3648		Elevation		Unit Ltr. - Sec. - TWP - Rge. 16 21S 36E			
Csg. Size 5 1/2	Wt. 15.5	d 4.950	Set At 3700	Perforations: From: 3458 To: 3595				County LEA			
Tbg. Size 2-3/8	Wt. 4.7	d 1.995	Set At 3400	Perforations: From: To:				Pool			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple single						Packer Set At none		Formation PENROSE			
Producing Thru TBG.		Reservoir Temp. °F 90		Mean Annual Temp. °F 60		Baro. Press - P _a 13.2		Connection AIR			
L 3526.5	H 3526.5	Gg .722	% CO ₂ 5.47	% N ₂ 1.86	% H ₂ S	Prover		Meter Run 2.067		Taps FLG.	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI						200				
1.	2.067 X	1.500	33	48	60	100		N/A		24 hrs.
2.										
3.										
4.										
5.										

RATE OF FLOW CALCULATIONS							
NO.	COEFFICIENT (24 HOUR)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg.	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	12.76	47.10	46.2	1.000	1.177	1.005	111
2.							
3.							
4.							
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1.	.07	520	1.35	.990	DRY GAS	
2.					A.P. L Gravity of Liquid Hydrocarbons DRY	Deg.
3.					Specific Gravity Separator Gas .722	XXXXXXXXXX
4.					Specific Gravity Flowing Fluid DRY	XXXXXX
5.					Critical Pressure 688	P.S.I.A.
					Critical Temperature 386	R

P_c **215.2** P_c² **46.5**

NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²
1.	12.8	141.8	20.1	25.4
2.				
3.				
4.				
5.				

1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.793$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1,275$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.793$

Absolute Open Flow 1,275	Mcf @ 15.025	Angle of Slope θ 45°	Slope, n 1.000
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Remarks: **NO FLUID MADE DURING TEST**

Approved By-Division

Conducted By:

PRO WELL TESTER

Calculated By:

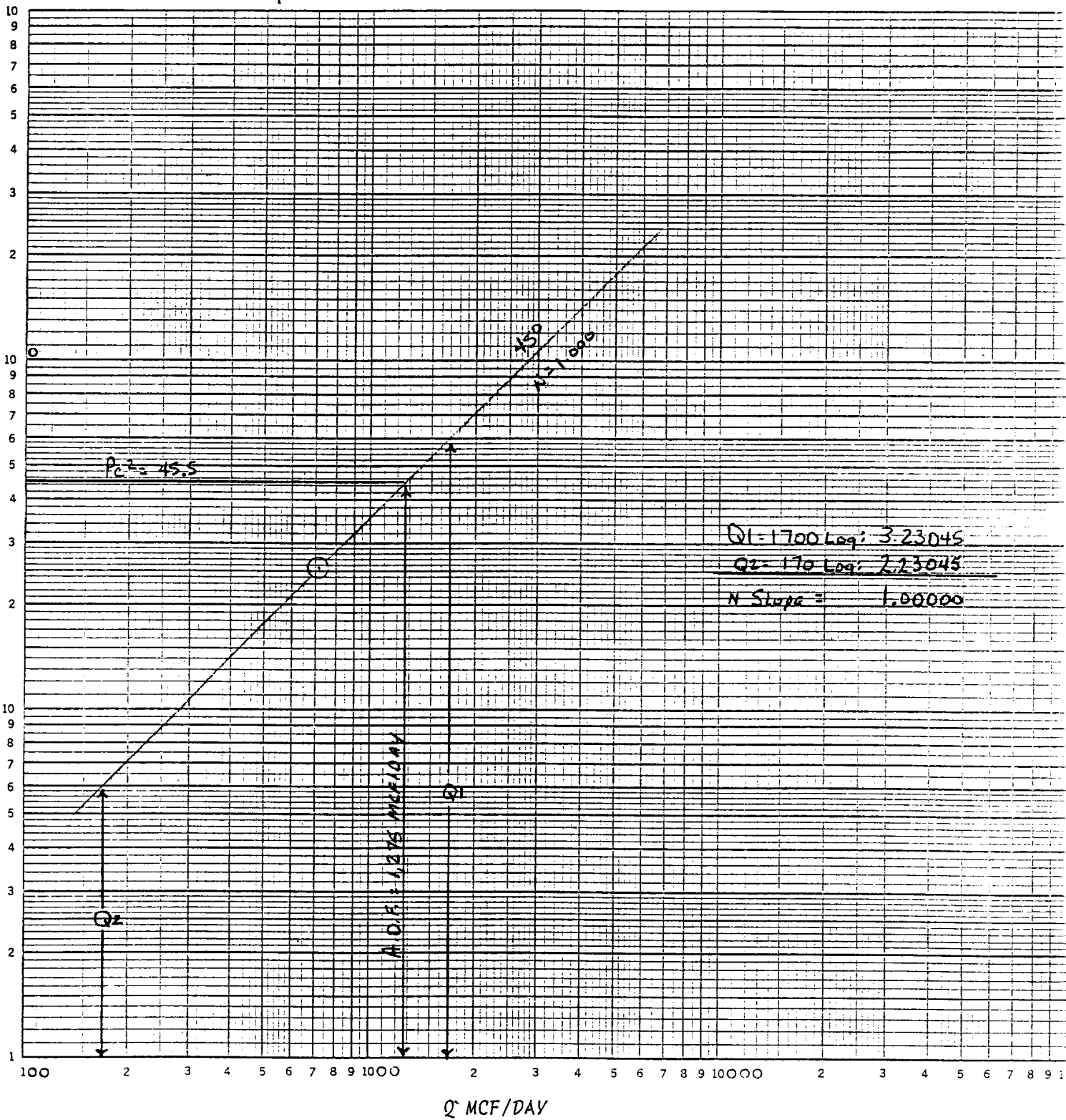
KS

Checked By:

NOV 13 1994

$P_C^2 - P_W^2 (x_{hsnds})$ 46 7400

KE LOGARITHMIC 3 X 3 CYCLES
KEUFFEL & ESSER CO. MADE IN U.S.A.



Laboratory Services, Inc.

1331 Tasker Drive
Hobbs, New Mexico 88240

Telephone: (505) 397-3713

FOR:

Pro Well Testing & Wireline
Attention: Mr. Leonard Abney
P. O. Box 791
Hobbs, New Mexico 88241

SAMPLE

IDENTIFICATION: Skelly "B" #3

COMPANY: Texaco E. & P. Inc.

LEASE:

PLANT:

SAMPLE DATA: DATE SAMPLED: 11-08-94 10:15AM GAS (XX) LIQUID ()
ANALYSIS DATE: 11-08-94 SAMPLED BY: Pro Well
PRESSURE - PSIG ANALYSIS BY: Rolland Perry
SAMPLE TEMP. °F
ATMOS. TEMP. °F 75.00

REMARKS:

COMPONENT ANALYSIS

COMPONENT	MOL PERCENT	GPM
Hydrogen Sulfide (H2S)		
Nitrogen (N2)	1.86	
Carbon Dioxide (CO2)	5.47	
Methane (C1)	80.31	
Ethane (C2)	6.42	1.713
Propane (C3)	3.47	0.954
i-Butane (IC4)	0.49	0.160
n-Butane (NC4)	1.02	0.321
i-Pentane (IC5)	0.29	0.106
n-Pentane (NC5)	0.24	0.087
Hexane Plus (C6)	0.43	0.176
	100.00	3.517
BTU/CU.FT. - DRY	1103	MOLECULAR WT. 20.9018
AT 14.650 DRY	1100	
AT 14.650 WET	1080	
AT 14.73 DRY	1105	
AT 14.73 WET	1086	
SPECIFIC GRAVITY -		
CALCULATED	0.722	
MEASURED		

Equivalent Diameter Program

Author: Bob Murray

Date: December 26, 1990

L1 =	3400 ft.	L5 =	0 ft.	Lt =	3526.5 ft.
D1 =	1.995 in.	D5 =	1 in.	C =	0.10797

L2 =	126.5 ft.	L6 =	0 ft.		
D2 =	4.95 in.	D6 =	1 in.		
				Deff =	2.009 in.

L3 =	0 ft.	L7 =	0 ft.	Fr =	0.01746
D3 =	1 in.	D7 =	1 in.		

L4 =	0 ft.	L8 =	0 ft.		
D4 =	1 in.	D8 =	1 in.		

UNIT : SECTION : 16 TOWNSHIP : 21
 L : 3526 H : 3526 L/H : 1 G/GMIX : 0.722
 %CO2 : 5.47 %N2 : 1.86 H2S : DATE : 11-08-94
 d : 2.009 Fr : 0.017901 GH : 2546.1 RANGE : 36

Pt2 = 12.8 Pw = 141.8 *
 0.0 ERR *
 0.0 ERR *
 0.0 ERR *

VOL 1 : 711 PSIA 1 : 113.2 RESV. TEMP 90.0
 VOL 2 : PSIA 2 :
 VOL 3 : PSIA 3 : SHUT-IN PR= 213.2
 VOL 4 : PSIA 4 :

Pc2-Pw2= 25.4 Pw2 = 20.1 *
 ERR ERR *
 ERR ERR *
 ERR ERR *

PCR : 688
 TCR : 386

n = 1.000

Pc2/(Pc2-Pw2) = 1.793
 ERR
 ERR
 ERR

LINE	RATE 1		RATE 2		RATE 3		RATE 4	
	'1ST	'2ND	'1ST	'2ND	'1ST	'2ND	'1ST	'2ND
1 QM	0.711	0.711	0.000	0.000	0.000	0.000	0.000	0.000
2 TW	534	534	534	534	534	534	534	534
3 Ts	550.0	550.0	550.0	550.0	550.0	550.0	550.0	550.0
4 T	542.0	542.0	542.0	542.0	542.0	542.0	542.0	542.0
PR (est)	0.16		0.00		0.00		0.00	
5 Z(est)	0.956	0.952	ERR	ERR	ERR	ERR	ERR	ERR
6 TZ	518.0	516.0	ERR	ERR	ERR	ERR	ERR	ERR
7 GH/TZ	4.915	4.935	ERR	ERR	ERR	ERR	ERR	ERR
8 eS	1.202	1.203	ERR	ERR	ERR	ERR	ERR	ERR
9 l-e-S	0.168	0.169	ERR	ERR	ERR	ERR	ERR	ERR
10 Pt	113.2	113.2	0.0	0.0	0.0	0.0	0.0	0.0
11 Pt2 /1000	12.8	12.8	0.0	0.0	0.0	0.0	0.0	0.0
12 Fr	0.017901	0.017901	0.017901	0.017901	0.017901	0.017901	0.017901	0.017901
13 Fc=FrTZ	9.273	9.237	ERR	ERR	ERR	ERR	ERR	ERR
14 FcQm	6.59	6.57	ERR	ERR	ERR	ERR	ERR	ERR
15 L/H(FcQm)	43.5	43.1	ERR	ERR	ERR	ERR	ERR	ERR
16 Fw	7.316957	7.285970	ERR	ERR	ERR	ERR	ERR	ERR
17 Pw2	20.1	20.1	ERR	ERR	ERR	ERR	ERR	ERR
18 Ps2	24.2	24.2	ERR	ERR	ERR	ERR	ERR	ERR
19 Ps	155.6	155.5	ERR	ERR	ERR	ERR	ERR	ERR
20 P	134.4	134.4	ERR	ERR	ERR	ERR	ERR	ERR
21 Pr	0.20	0.20	ERR	ERR	ERR	ERR	ERR	ERR
22 Tr	1.40	1.40	1.40	1.40	1.40	1.40	1.40	1.40
23 Z	0.952	0.952	ERR	ERR	ERR	ERR	ERR	ERR

[Pc2/(Pc2-Pw2)]n = 1.793
 ERR
 ERR
 ERR

AOF= Q 1.275
 ERR
 ERR
 ERR

FORM C122-D