Submit in duplicate to appropriate district office.
See Rule 401 & Rule 1122

State of New Mexico
Energy Minerals and Natural Resources
Oil Conservation Division
2040 South Pacheco
Santa Fe, NM 87505

Form C-122
Revised October, 1999

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator	PHILLIPS PETROLEUM COMPANY					Lease or Unit Name	CORNER POCKET 14 STATE		
Type Test ☑ Initial ☐ Annual ☐ Special						Test Date 4/1/02	Well No. 1		
Completion Date 3/11/02	Total Depth 12900			Plug Back TD 12572		Elevation 3669 GL	Unit Ltr - Sec - TWP - Rge A 14 21 34		
Csg. Size 4 1/2	Wt. 13.5	d 3.92	Set At 12898	Perforations: From: 12128	To: 12136		County LEA		
Tbg. Size 2 3/8	Wt. 4.7	d 1.995	Set At 11994	Perforations: From: OPEN	To: ENDED		Pool WILSON		
Type Well-Single-Bradenhead-G.G. or G.O. Multiple SINGLE				Packer Set At 11401			Formation ATOKA		
Producing Thru Tbg. Size	Reservoir Temp.°F 169.0 @ 12132		Mean Annual Temp. °F 60	Baro. Press.-P_a 13.2			Connection CONOCO		

L	H	Gg	%CO_2	%N_2	%H_2S	Prover	Meter Run	Taps
12132	12132	0.648	0.285	1.049	N/A	N/A	3.068	FLG

	FLOW DATA				TUBING DATA		CASING DATA		
No.	Prover Line Size x Orifice Size	Press p.s.i.g.	Diff. h_w	Temp. °F	Press p.s.i.g.	Temp. °F	Press p.s.i.g.	Temp. °F	Duration of Flow
SI					2265		PKR		72 HRS
1	3 X .750	731	10.5	68	1305		"		1 HR
2									
3									
4									
5									

RATE OF FLOW CALCULATIONS

No.	COEFFICIENT (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor F_g	Super Compress Factor F pv	Rate of Flow Q. Mcfd
1							320
2							
3	MEASURED	BY	TOTAL		FLOW	METER	
4							
5							

No.	P_r	Temp. °R	T_r	Z
1				
2				
3		N/A		
4				
5				

Gas Liquid Hydrocarbon Ratio DRY GAS Mcf bbl.
A.P. I. Gravity of Liquid Hydrocarbons DRY Deg.
Specific Gravity Separator Gas 0.648 XXXXXXX
Specific Gravity Flowing Fluid XXXXX
Critical Pressure 669 P.S.I.A. ____ P.S.I.A.
Critical Temperature 369 R. ____ R

P_c * 3067.9 P_c2 * 9412.0

No.	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		2713.9	7365.2	2046.8
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$ 4.598 (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n =$ 4.598

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n =$ 1.471

79825

Absolute Open Flow 1,471 Mcfd @ 15.025 Angle of Slope θ: 45 Slope n: 1

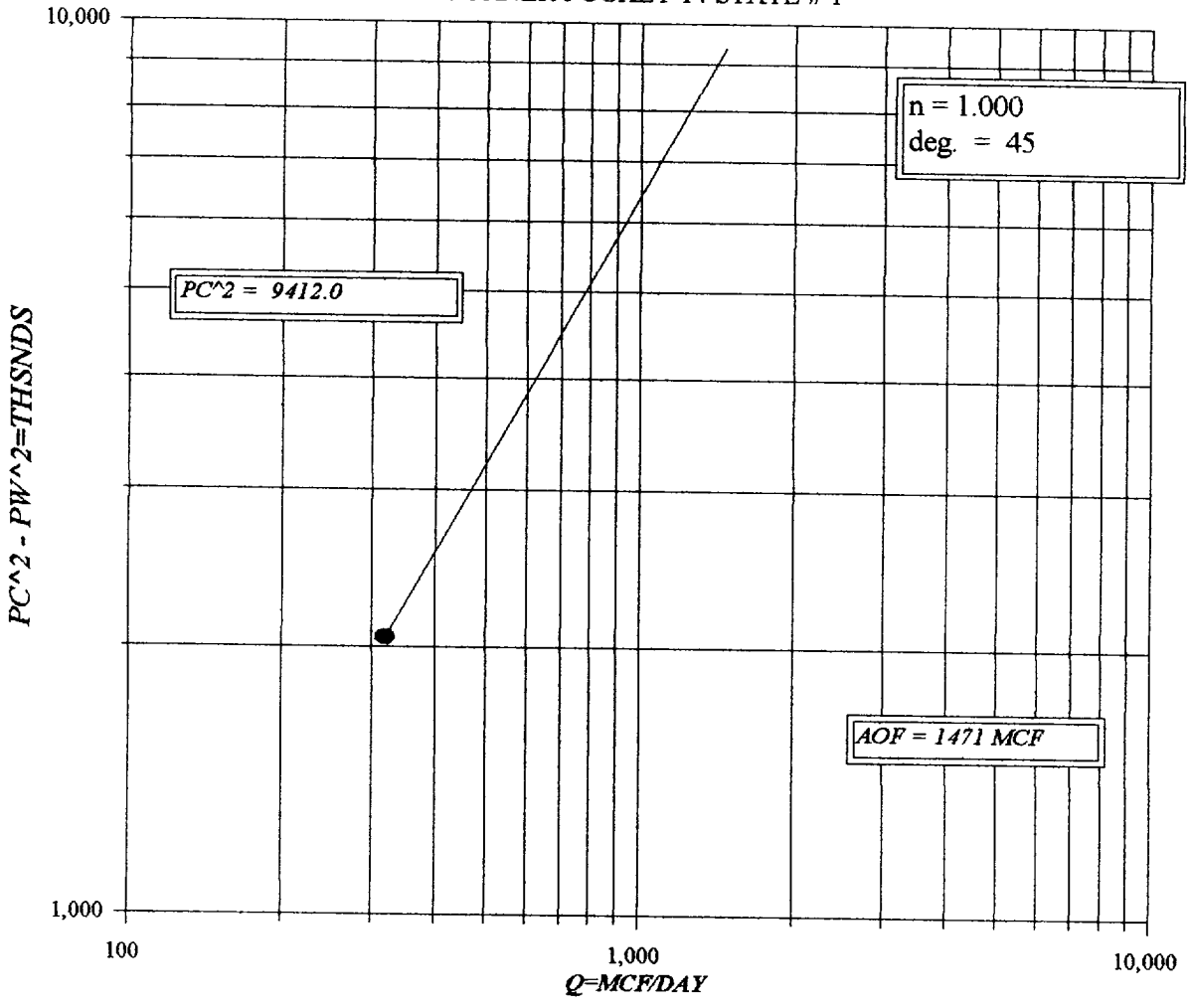
Remarks: * BHP'S USED TO CALCULATE TEST - NO FLUID PRODUCED

Approved By Division: ORIGINAL SIGNED BY PAUL F. KAUTZ PETROLEUM ENGINEER
Conducted By: JARREL SERVICES, INC.
Calculated By: BM
Checked By: BM

APR 09 2002

PHILLIPS PETROLEUM COMPANY

CORNER POCKET 14 STATE # 1



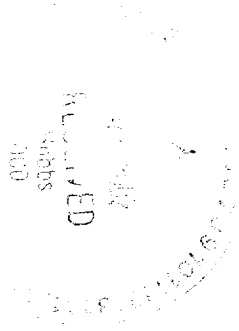
WORK SHEET FOR CALCULATION OF WELLHEAD PRESSURE (Pc ~~Pw~~)
FROM KNOWN BOTTOM HOLE PRESSURE (Pf or Ps)

FORM C-122F

COMPANY PHILLIPS PETRO. CO. LEASE :C.P.14 ST. WELL NO. : 1 DATE 4-01-02
UNIT A SECTION : 14 TWNSHP : 21 RANGE : 34
L 12132 H : 12132 L/H : 1 G/GMIX : 0.6480
CO2 : 0.285 N2 : 1.049 H2S :
GH : 7861.5 PCR : 669 TCR : 369

LINE		1	2	3	4	5	6	7	8
1	TW(W.H. R)	534	534	534	534	534	534	534	534
2	Ts(B.H. R)	655.3	655.3	655.3	655.3	655.3	655.3	655.3	655.3
3	T=(Tw+Ts/2)	594.7	594.7	594.7	594.7	594.7	594.7	594.7	594.7
4	Z (EST.)	0.946	0.851	ERR	ERR	ERR	ERR	ERR	ERR
5	TZ	562	506	ERR	ERR	ERR	ERR	ERR	ERR
6	GH/TZ	13.977	15.540	ERR	ERR	ERR	ERR	ERR	ERR
7	eS(TABLE XIV)	1.689	1.791	ERR	ERR	ERR	ERR	ERR	ERR
8	Pf or Ps	4105.7	4105.7	0	0	0	0	0	0
9	Pf2 or Ps2	16856.8	16856.8	0.0	0.0	0.0	0.0	0.0	0.0
10	Pc2=Pf/eS or Pw2=Ps2/eS	9980.4	9412.0	ERR	ERR	ERR	ERR	ERR	ERR
11	Pc or Pw	3159	3068	ERR	ERR	ERR	ERR	ERR	ERR
12	P=(Pw+Ps/2)or(Pc+Pf/2)	3632	3587	ERR	ERR	ERR	ERR	ERR	ERR
13	Pr=(P/Pcr)	5.43	5.36	ERR	ERR	ERR	ERR	ERR	ERR
14	Tr(T/Tcr)	1.61	1.61	1.61	1.61	1.61	1.61	1.61	1.61
15	Z (TABLE XI)	0.851	0.848	ERR	ERR	ERR	ERR	ERR	ERR

Pc ~~Pw~~ 1 : 3067.9 PW 2 : ERR PW 3 : ERR PW 4 : ERR



WORK SHEET FOR CALCULATION OF WELLHEAD PRESSURE ~~(Pc or~~ Pw)
FROM KNOWN BOTTOM HOLE PRESSURE (Pf or Ps)

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GH : 7861.5 PCR : 669 TCR : 369

LINE		1	2	3	4	5	6	7	8
1	TW(W.H. R)	534	534	534	534	534	534	534	534
2	Ts(B.H. R)	655.3	655.3	655.3	655.3	655.3	655.3	655.3	655.3
3	T=(Tw+Ts/2)	594.7	594.7	594.7	594.7	594.7	594.7	594.7	594.7
4	Z (EST.)	0.915	0.829	ERR	ERR	ERR	ERR	ERR	ERR
5	TZ	544	493	ERR	ERR	ERR	ERR	ERR	ERR
6	GH/TZ	14.452	15.940	ERR	ERR	ERR	ERR	ERR	ERR
7	eS(TABLE XIV)	1.719	1.818	ERR	ERR	ERR	ERR	ERR	ERR
8	Pf or Ps	3659.2	3659.2	0	0	0	0	0	0
9	Pf2 or Ps2	13389.7	13389.7	0.0	0.0	0.0	0.0	0.0	0.0
10	Pc2=Pf/eS or Pw2=Ps2/eS	7787.5	7365.1	ERR	ERR	ERR	ERR	ERR	ERR
11	Pc or Pw	2791	2714	ERR	ERR	ERR	ERR	ERR	ERR
12	P=(Pw+Ps/2)or(Pc+Pf/2)	3225	3187	ERR	ERR	ERR	ERR	ERR	ERR
13	Pr=(P/Pcr)	4.82	4.76	ERR	ERR	ERR	ERR	ERR	ERR
14	Tr(T/Tcr)	1.61	1.61	1.61	1.61	1.61	1.61	1.61	1.61
15	Z (TABLE XI)	0.829	0.828	ERR	ERR	ERR	ERR	ERR	ERR

PW 1 : 2713.9 PW 2 : ERR PW 3 : ERR PW 4 : ERR

Laboratory Services, Inc.

4016 Fiesta Drive
Hobbs, New Mexico 88240

Telephone: (505) 397-3713

FOR: Jarrel Services Inc.
Attention: Mr. Donnie Dickerson
P. O. Box 1230
Hobbs, New Mexico 88240

SAMPLE:
IDENTIFICATION: Corner Pocket 14 St. #1
COMPANY: Phillips Petroleum Co.
LEASE:
PLANT:

SAMPLE DATA:
DATE SAMPLED: 4/1/02
ANALYSIS DATE: 4/2/02
PRESSURE – PSIG
SAMPLE TEMP. °F
ATMOS. TEMP. °F

GAS (XX) LIQUID ( )
SAMPLED BY: Donnie Dickerson
ANALYSIS BY: Vickie Biggs

REMARKS:

COMPONENT ANALYSIS

COMPONENT		MOL PERCENT	GPM
Hydrogen Sulfide	(H2S)		
Nitrogen	(N2)	1.049	
Carbon Dioxide	(CO2)	0.285	
Methane	(C1)	88.653	
Ethane	(C2)	5.646	1.506
Propane	(C3)	2.309	0.635
I-Butane	(IC4)	0.363	0.118
N-Butane	(NC4)	0.743	0.234
I-Pentane	(IC5)	0.239	0.087
N-Pentane	(NC5)	0.244	0.088
Hexane Plus	(C6+)	0.469	0.204
		100.000	2.872

BTU/CU.FT. – DRY	1131
AT 14.650 DRY	1128
AT 14.650 WET	1108
AT 14.73 DRY	1134
AT 14.73 WET	1114
SPECIFIC GRAVITY – CALCULATED	0.648
MEASURED	

MOLECULAR WT. 18.7803