## NEW MEXICO OIL CONSERVATION COMMISSION

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Corrected Copy MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS Revised 12-1-55												
Pool Jalmat				Formation Yates - 7 Rivers				County Lea				
InitialAnnualSpecialDate of Test 10-22 to 10-26-56												
							Well No1					
Unit O Sec. 25 Twp. 22-S Rge. 36-E Purchaser El Paso Natural Gas Co.												
Casing 5 Wt. 15.5 I.D Set at 2920 Perf To												
					Set at Perf			То				
Gas Pay: From 3130 To 3450												
Producing Thru: Casing <b>x</b> Tubing Type Well <b>Single</b> Single-Bradenhead-G. G. or G.O. Dual												
Date	e of Complet	ion: 12-	24-50	Packe	Single-Br Packer None Rese				denhead-G. G. or G.O. Dual voir Temp			
Duoc	of comprov					ED DATA						
Tested Through (Prover) (Choke) (Meter) Type Taps												
Test				/ [Meter/		Tubing	Data	Casing Data				
T	(THE GODDAY	Flor (Cheke	Pres	s. Diff.	Temp.		Temp.		Temp.	Duration of Flow		
No.	(Line) Size	(Orific) Size	e)     psi	g h <sub>w</sub>	°F.	psig	°F.	psig	<sup>э</sup> ғ.	Hr.		
SI		1.250	719	2.12	71			827 719		72 24		
$\frac{1}{2}$ . $\frac{3}{4}$ . $\frac{4}{5}$ .	<u> </u>	1.25		2,85	71			669 625		24		
3.	4	1.25		3.6	68		<u> </u>	505				
5.1							l					
FLOW CALCULATIONS												
No.	Coeffici	efficient		Pressure		Temp. tor	Gravity Factor	Compre Facto	t i i	Rate of Flow Q-MCFPD		
NO.	Flg (24-Hou	$\mathbf{r}$ ) $$	hwpf	psia	- F	t	Fg_	<sup>F</sup> p <b>v</b>		@ 15.025 psia		
1.	9.643	9.643 9.643 9.643			. 989	6	.9463	1.080		<u>554</u> 721		
1. 2. 3.	9.643	9.643				715 •74		1.0	69	880		
$\frac{2^{\circ}}{4^{\circ}}$	9.643		90.93 105.07		.989 .991 .992	4	.9463 .9463 .9463	1.0	66	1.014		
4.												
				PR	ESSURE (	ALCULATI	ONS					
las I	Liquid Hydro	carbon R	atio Dr	w Gas	cf/bbl.		Spec:	ific Gravi	ty Sepa	arator Gas		
Gas Liquid Hydrocarbon Ratio <u>Dry Ga</u> Gravity of Liquid Hydrocarbons					deg. Spe				cific Gravity Flowing Fluid 840.2 P <sup>2</sup> 705.9			
<sup>F</sup> c	.9171	<u></u>	(1-e <sup>-5</sup>	•) .126		-	Pc	34 <b>0</b> ,2	_P <u>c70</u>	2•Y		
		·	r		<del></del>			1				
No.	Pw	$P_t^2$	F <sub>c</sub> Q	(F <sub>c</sub> Q) <sup>2</sup>	2 (1	$\left[\frac{r_{cQ}}{c^{-s}}\right]^{2}$	P <sub>w</sub> 2	$P_c^2 - P_w^2$	Ca	$\begin{array}{c c} \mathbf{A1.} & \mathbf{P_W} \\ \mathbf{P_U} & \mathbf{P_C} \end{array}$		
	🕱 (psia)	Ĭ		· ·					F			
<u>1</u>	732.2	536.1	0.5	0.3		.06	536.1	169.8 240.4		-8715 -8119		
2. 3.	638.2	407.3	0,8	0,6		.08	407.4	298.5		•75%		
<u>J.</u> 4.	598.2	357.8	0.9	0,8		.10	357.9	348.0		.7120		
5.												
Absolute Potential: 2,000 MCFPD; n COMPANY Dalport Oil Corporation												
	PANY	Dalpor	t ULL CO	nion 1.4fe	Bldg. D	allas. T	exas			<u></u>		
ADDRESS 930 Fidelity Union Life Bldg, Dallas, Texas AGENT and TITLE Acquarter production Manager												
- WT (P	NESSED	Smith	6 Rinner									
COM	PANY EL	raso Nat	ural Gas	vonipany	סס	MARKS						
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## **INSTRUCT JONS**

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Contribution at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

- Q = Actual rate of flow at end of flow period at W. H. working pressure  $(P_W)$ . MCF/da. @ 15.025 psia and 60° F.
- PcI 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- Pw Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- P<sub>f</sub> Meter pressure, psia.
- $h_w$  Differential méter pressure, inches water.
- FgI Gravity correction factor.

Ft Flowing temperature correction factor.

 $F_{pv}$ : Supercompressability factor.

n \_ Slope of back pressure curve.

Note: If  $P_W$  cannot be taken because of manner of completion or condition of well, then  $P_W$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_{\chi}$ .