

## NEW MEXICO OIL CONSERVATION COMMISSION

HOBBS OFFICE OCC

Form C-122

Revised 12-1-55

## MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Pool Jalmat Formation Yates & Seven Rivers County Lea  
Initial \_\_\_\_\_ Annual X Special \_\_\_\_\_ Date of Test 3-7-58  
Company Continental Oil Company Lease Meyer A-29 Well No. 1  
Unit 0 Sec. 29 Twp. 22 Rge. 36 Purchaser El Paso Nat. Gas Company  
Casing 7" Wt. 17 I.D. \_\_\_\_\_ Set at 3390 Perf. 3100 To 3390  
Tubing None Wt. \_\_\_\_\_ I.D. \_\_\_\_\_ Set at \_\_\_\_\_ Perf. \_\_\_\_\_ To \_\_\_\_\_  
Gas Pay: From 3100 To 3390 L 3100 xG .665 -GL 2062 Bar.Press. 13.2  
Producing Thru: Casing X Tubing \_\_\_\_\_ Type Well Single  
Single-Bradenhead-G. G. or G.O. Dual  
Date of Completion: 12-24-53 Packer None Reservoir Temp. 900

## OBSERVED DATA

Tested Through (Packer) (Casing) (Meter) Type Taps Flange

| No. | Flow Data   |                |             |                      |           | Tubing Data |           | Casing Data |           | Duration of Flow Hr. |
|-----|-------------|----------------|-------------|----------------------|-----------|-------------|-----------|-------------|-----------|----------------------|
|     | (Line) Size | (Orifice) Size | Press. psig | Diff. h <sub>w</sub> | Temp. °F. | Press. psig | Temp. °F. | Press. psig | Temp. °F. |                      |
| 1.  | 4"          | 1.000          | 454         | 6.25                 | 48        |             |           | 626         |           | 72                   |
| 2.  |             |                |             |                      |           |             |           | 465         |           | 24                   |
| 3.  |             |                |             |                      |           |             |           |             |           |                      |
| 4.  |             |                |             |                      |           |             |           |             |           |                      |
| 5.  |             |                |             |                      |           |             |           |             |           |                      |

## FLOW CALCULATIONS

| No. | Coefficient<br>Flange<br>(24-Hour) | $\sqrt{h_w P_f}$ | Pressure<br>psia | Flow Temp.<br>Factor<br>F <sub>g</sub> | Gravity<br>Factor<br>F <sub>g</sub> | Compress.<br>Factor<br>F <sub>pv</sub> | Rate of Flow<br>Q-MCFPD<br>@ 15.025 psia |
|-----|------------------------------------|------------------|------------------|--|-------------------------------------|--|--|
| 1.  | 6.135                              | 54.03            | 467.2            | .9498                                  | 1.0117                              | 1.057                                  | 336                                      |
| 2.  |                                    |                  |                  |  |                                     |  |  |
| 3.  |                                    |                  |                  |  |                                     |  |  |
| 4.  |                                    |                  |                  |  |                                     |  |  |
| 5.  |                                    |                  |                  |  |                                     |  |  |

## PRESSURE CALCULATIONS

Gas Liquid Hydrocarbon Ratio Dry cf/bbl.  
Gravity of Liquid Hydrocarbons \_\_\_\_\_ deg.  
P<sub>c</sub> .4682 (1-e<sup>-s</sup>) .132

Specific Gravity Separator Gas .665  
Specific Gravity Flowing Fluid \_\_\_\_\_  
P<sub>c</sub> 639.2 P<sub>c</sub> 408.6

| No. | P <sub>t</sub> (psia) | P <sub>t</sub> <sup>2</sup> | F <sub>c</sub> Q | (F <sub>c</sub> Q) <sup>2</sup> | (F <sub>c</sub> Q) <sup>2</sup><br>(1-e <sup>-s</sup> ) | P <sub>w</sub> <sup>2</sup> | P <sub>c</sub> <sup>2</sup> -P <sub>w</sub> <sup>2</sup> | Cal.<br>P <sub>w</sub> | P <sub>w</sub><br>P <sub>c</sub> |
|-----|-----------------------|-----------------------------|------------------|---------------------------------|---|-----------------------------|--|------------------------|----------------------------------|
| 1.  | 478.2                 | 228.7                       | .157             | .025                            | .003  | 228.7                       | 179.9  | 478.2                  | 74.81                            |
| 2.  |                       |                             |                  |                                 |   |                             |  |                        |                                  |
| 3.  |                       |                             |                  |                                 |   |                             |  |                        |                                  |
| 4.  |                       |                             |                  |                                 |   |                             |  |                        |                                  |
| 5.  |                       |                             |                  |                                 |   |                             |  |                        |                                  |

Absolute Potential: 630 MCFPD; n .771  
COMPANY Continental Oil Company  
ADDRESS Box 68, Eunice, New Mexico  
AGENT and TITLE J. B. P.  
WITNESSED \_\_\_\_\_  
COMPANY \_\_\_\_\_

## REMARKS

During the regular Multi-point testing schedule, a rate of flow could not be obtained. However, the data used here was taken from the deliverability test conducted 3-7-58 and the average Jalmat slope of .771 drawn thru highest rate of flow.

NMOCC-3 EWW HLJ RLA File-2

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

- $Q$  = Actual rate of flow at end of flow period at W. H. working pressure ( $P_w$ ).  
MCF/da. @ 15.025 psia and 60° F.
- $P_c$  = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater.  
psia
- $P_w$  = Static wellhead working pressure as determined at the end of flow period.  
(Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- $P_t$  = Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- $P_f$  = Meter pressure, psia.
- $h_w$  = Differential meter pressure, inches water.
- $F_g$  = Gravity correction factor.
- $F_t$  = Flowing temperature correction factor.
- $F_{pv}$  = Supercompressability factor.
- $n$  = Slope of back pressure curve.

Note: If  $P_w$  cannot be taken because of manner of completion or condition of well, then  $P_w$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_t$ .