NEW MEXICO OIL CONSERVATION COMMISSION

Form C-122

Revised 12-1-55

MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Pool **Blinebry Gas** Formation **Blinebry** County **Lea**

Initial ____ Annual **X** Special ____ Date of Test **8 - 1/9 - 1957**

Company **The Ohio Oil Company** Lease **Lou Worthan** Well No. **9**

Unit **E** Sec. **11** Twp. **22-S** Rge. **37-E** Purchaser **Permian Basin Pipeline Company**

Casing **5½"** Wt. **17.0#** I.D. **4.892"** Set at **6417'** Perf. **5330 5455** To **5430 5505**

Tubing **2-3/8"** Wt. **4.7** I.D. **1.995"** Set at **6133** Perf. **6066** To **6068**

Gas Pay: From **5330'** To **5505'** L **5330'** xG ____ -GL **See Below** Bar.Press. **13.2**

Producing Thru: Casing **X** Tubing ____ Type Well **Gas-Gas Dual**
Single-Bradenhead-G. G. or G.O. Dual

Date of Completion: **5-15-57** Packer **5692'** Reservoir Temp. **--**

OBSERVED DATA

Tested Through ~~(Prover)~~ ~~(Choke)~~ (Meter) Type Taps **Pipe**

CO_2 = 0.00% **N_2 = 2.30%**

No.	Flow Data ~~(Prover)~~ (Line) Size	Flow Data ~~(Choke)~~ (Orifice) Size	Flow Data Press. psig	Flow Data Diff. h_w	Flow Data Temp. °F.	Tubing Data Press. psig	Tubing Data Temp. °F.	Casing Data Press. psig	Casing Data Temp. °F.	Duration of Flow Hr.
SI						Packer	--	1762.3		72 hr SIP
1.	4"	2.25	480.3	5.3	84	"	--	1608.4	84	24 hrs
2.	4"	2.25	489.2	12.0	63	"	--	1516.4	63	24 hrs
3.	4"	2.25	490.0	26.3	64	"	--	1363.2	64	24 hrs
4.	4"	2.25	494.2	43.7	64	"	--	1210.4	64	24 hrs
5.										

FLOW CALCULATIONS

No.	Coefficient (24-Hour)	$\sqrt{h_w p_f}$	Pressure psia	Flow Temp. Factor F_t	Gravity Factor F_g	Compress. Factor F_{pv}	Rate of Flow Q-MCFPD @ 15.025 psia
1.	40.53	51.14	493.5	0.9777	0.9359	1.047	1986
2.	40.53	77.65	502.4	0.9971	0.9359	1.055	3098
3.	40.53	115.04	503.2	0.9962	0.9359	1.056	4591
4.	40.53	148.91	507.4	0.9962	0.9359	1.056	5942
5.							

PRESSURE CALCULATIONS

Gas Liquid Hydrocarbon Ratio **See Below** cf/bbl.
Gravity of Liquid Hydrocarbons **71.0** deg. **API**
F_c **1.812** $(1-e^{-s})$ **See Below**

Specific Gravity Separator Gas **0.685**
Specific Gravity Flowing Fluid **See Below**
P_c **1775.5** P_c^2 **3152.4**

No.	P_w / P_t (psia)	P_t^2	F_cQ	$(F_cQ)^2$	$\frac{(F_cQ)^2}{(1-e^{-s})}$	P_w^2	$P_c^2-P_w^2$	Cal. P_w	$\frac{P_w}{P_c}$
1.	1621.6	2629.6	3.599	12.95	2.99	2632.6	519.8	1622.5	0.91
2.	1529.6	2339.7	5.614	31.52	7.28	2347.0	805.4	1532.0	0.86
3.	1376.4	1894.5	8.319	69.21	16.13	1910.6	1241.8	1382.2	0.78
4.	1223.6	1497.2	10.767	115.93	26.90	1524.1	1628.3	1234.5	0.70
5.									

Absolute Potential: **11,185** MCFPD; n **0.957481**

COMPANY **The Ohio Oil Company**

ADDRESS **Box 2107, Hobbs, New Mexico**

AGENT and TITLE **Harrell D. Chiles - Petroleum Engr.** Harrell D. Chiles

WITNESSED **Mr. R. L. West**

COMPANY **Permian Basin Pipeline Company**

REMARKS

Rate	(Bbls) Fluid	(ft^3/bbl) GLR	Gmix	GL	$(1-e^{-s})$
1	26.66	74,494	0.717	3822'	0.231
2	39.40	78,629	0.716	3816'	0.231
3	72.14	63,640	0.722	3848'	0.233
4	86.26	68,885	0.720	3838'	0.232

INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

NOMENCLATURE

Q = Actual rate of flow at end of flow period at W. H. working pressure (P_w). MCF/da. @ 15.025 psia and 60° F.

P_c = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia

P_w = Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia

P_t = Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia

P_f = Meter pressure, psia.

h_w = Differential meter pressure, inches water.

F_g = Gravity correction factor.

F_t = Flowing temperature correction factor.

F_{pv} = Supercompressability factor.

n = Slope of back pressure curve.

Note: If P_w cannot be taken because of manner of completion or condition of well, then P_w must be calculated by adding the pressure drop due to friction within the flow string to P_t.