

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 10-21-68			
Company TEXACO Inc.				Connection Northern Natural					
Well Blindbry				Formation Blindbry Gas				Unit	
Completion Date 1-20-54		Total Depth 7124		Packer Back Vt 7124		Elevation 3371 DF		Name of Owner A. H. Blindbry Fed. NCT-1	
Gas Size 5.5	Wt. 17	d 4.892	Set At 7124	Perforations: From 5563 To 5675		Well No. 6			
Tbg. Size 2.0625	Wt. 3.40	d 1.750	Set At 5671	Perforations: From _____ To _____		Unit Sec. Twp. Rge. B 19 22-S 38-E			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple G. O. Multiple						Packer Set At 5712		County Lea	
Producing Thru Tubing		Reservoir Temp. °F 570 @ 5563		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2		State New Mexico	
L 5563	H 5563	Gg 0.692	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run X	Taps Pine	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							961.0		Packer		72+
1.	4		1.750	483	1.0	67	882.5	60			1
2.	"		"	487	2.6	67	859.5	60			1
3.	"		"	489	6.4	67	730.2	60			1
4.	"		"	489	12.9	67	597.0	60			1
5.											

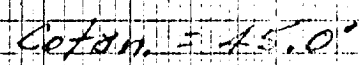
RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor Fpv	Rate of Flow Q, Mcfd
1	16.80	22.27	469.2	0.9933	1.205	1.060	474
2	"	36.07	500.2	"	"	"	769
3	"	56.70	502.2	"	"	"	1209
4	"	80.49	502.2	"	"	"	1715
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1	.75	520	1.37	1.060	176	
2.	.75	520	1.37	1.060	A.P.I. Gravity of Liquid Hydrocarbons	37.0 Deg.
3.	.75	520	1.37	1.060	Specific Gravity Separator Gas	0.680 XXXXXXXX
4.	.75	520	1.37	1.060	Specific Gravity Flowing Fluid	XXXXXX
5.					Critical Pressure	669 P.S.I.A.
					Critical Temperature	388 R
						949.1

NO.	P _r ²	P _w	P _w ²	P _r ² - P _w ²	(1) $\frac{P_r^2}{P_r^2 - P_w^2} = 2.778$	(2) $\left[\frac{P_r^2}{P_r^2 - P_w^2} \right]^n = 2.778$
1	802.3		810.5	138.6		
2	761.8		783.4	165.7		
3	552.3		607.4	341.7		
4	372.3		486.3	462.8		
5						

Absolute Open Flow		3,359 Mcfd @ 15.025	Angle of Slope θ	45.0°	Slope, n	1.000
Remarks:						
Approved By Commission: <i>[Signature]</i>						
Conducted By:		C. J. Seals	Calculated By:		C. J. Seals	Checked By:
<i>C. J. Seals</i>						

October 21, 1968



NOF 3,351

WORKSHEET FOR CALCULATION OF STATIC COLUMN WELLHEAD PRESSURE (P_w)

Form C-122D
Adopted 9-1-65

COMPANY Teneco, Inc. LEASE A.H. Whiskey Field WELL NO. 6 DATE 10-21-68

LOCATION: Unit B Section 19 Township 22-S Range 38-E

L 5563 H 5563 L/H 1.000 G 0.672 % CO₂ — % N₂ — % H₂S —

d 1.760 F_i .025671 GH 3850 P_{CT} 669 T_{CT} 388

1st Rate 2nd Rate 3rd Rate 4th Rate TABLE IX & X

LINE	1 st Trial	2 nd Trial	1 st Trial	2 nd Trial	1 st Trial	2 nd Trial	1 st Trial	2 nd Trial
1 Q _m	.414	—	.769	—	1.209	—	1.715	—
2 T _w (W.H. °R)	520	—	520	—	520	—	520	—
3 T _s (B.H. °R)	570	—	570	—	570	—	570	—
4 T = (T _w + T _s)	545	—	545	—	545	—	545	—
5 Z (Est.)	.869	.824	.830	.826	.830	.846	.862	.868
6 TZ	473.6	449.1	452.4	450.2	452.4	461.1	469.8	473.1
7 GH/TZ	8.129	5.573	5.510	6.552	6.510	6.350	6.195	6.138
8 e ^S (Table XIV)	1.356	1.375	1.376	1.378	1.376	1.368	1.360	1.357
9 1 - e ^S (Table XIV)	.263	.275	.273	.274	.273	.269	.265	.263
10 P _t	895.7	—	872.8	—	743.2	—	610.2	—
11 P _t 2/1000	602.3	—	761.8	—	552.3	—	372.3	—
12 F _t (Table XV)	.025671	—	.025671	—	.025671	—	.025671	—
13 F _c = F _t TZ	12.16	11.53	11.61	11.56	11.61	11.84	12.06	12.14
14 F _c Q _m	5.763	5.465	8.731	8.687	14.04	14.31	20.68	20.82
15 F _c /H (F _c Q _m) ²	33.21	29.67	79.76	78.98	197.1	204.8	427.7	433.5
16 F _w = L/H (F _c Q _m) ² (1 - e ^S)	9.7	8.2	21.8	21.6	53.8	55.1	113.3	114.0
17 P _w ² = P _t ² + F _w	811.0	810.5	782.6	783.4	606.1	607.4	485.6	486.3
18 P _s ² = e ^S P _w ²	1002.7	1114.4	1678.2	1078.5	234.0	230.7	660.4	659.7
19 P _s	1005.4	1055.7	1038.4	1037.0	713.3	711.6	812.7	812.3
20 P = (P _s ² + P _w ²)	2112.2	2112.1	2255.4	2255.9	228.3	227.4	711.5	711.3
21 P _z = (P/P _{CT})	1.45	1.16	1.43	1.43	1.34	1.34	1.16	1.06
22 T _z = (T/T _{CT})	1.40	—	1.40	—	1.40	—	1.40	—
23 P _z (Table XI)	1.84	1.83	1.83	1.83	1.84	1.84	1.83	1.83