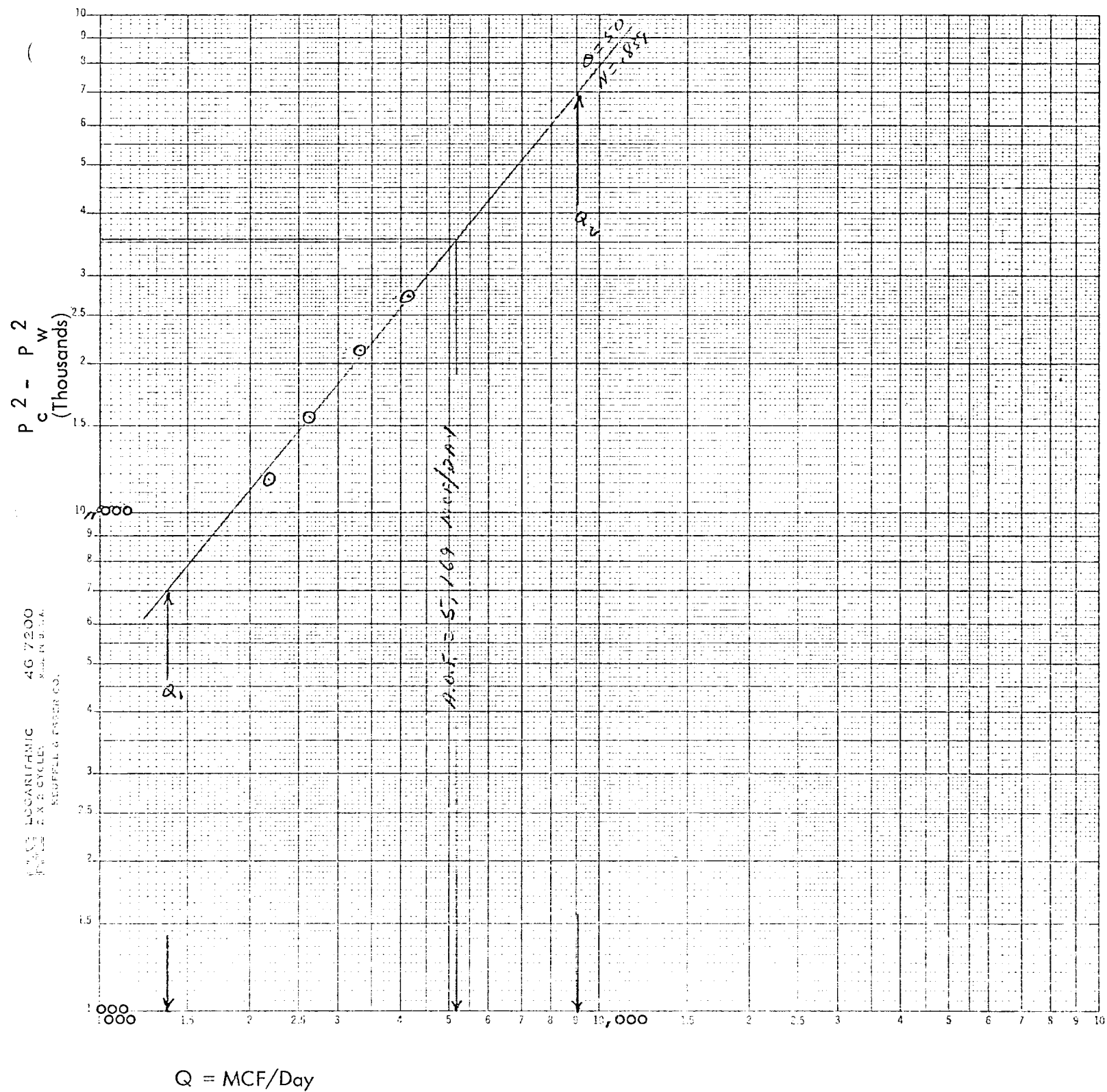


Texas West Oil & Gas Corp.
 State 35 # 1
 35-23-34
 Lea County, New Mexico
 1-9-74



**NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL**

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 1-9-74			
Company Texas West Oil & Gas Corp.				Connection None					
Pool Antelope Ridge				Formation Morrow				Unit	
Completion Date 1-5-74		Total Depth 13,865		Plug Back TD 13,826		Elevation 3462 GL		Farm or Lease Name State-35	
Csg. Size 7 5/8-5 1/2	Wt. 29.7-26.0	d 5.140	Set At 13,864	Perforations: From 13,305 To 13,538		Well No. 1			
Tbg. Size 2 7/8	Wt. 6.5	d 2.441	Set At 12,928	Perforations: From open To end		Unit Sec. Twp. Rge. K 35 23 34			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single						Packer Set At 12,920'		County Lea	
Producing Thru X		Reservoir Temp. °F 170 @ 13,305 (assumed)		Mean Annual Temp. °F		Baro. Press. - P _a		State New Mexico	
L 2,928	H 12,928	G _g .595	% CO ₂ .72	% N ₂	% H ₂ S .03	Prover	Meter Run 4"	Taps Flg.	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
SI							5945'			
1.	4 x 2.250			500	8.00	81	4853	63		
2.	4 x 2.250			510	11.50	79	4432	68		
3.	4 x 2.250			510	18.50	76	3716	70		
4.	4 x 2.250			510	28.50	73	2777	70		
5.										

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	25.64	64.07	513.2	.9804	1.296	1.040	2,171
2	25.64	77.57	523.2	.9822	1.296	1.041	2,636
3	25.64	98.38	523.2	.9850	1.296	1.041	3,352
4	25.64	122.11	523.2	.9877	1.296	1.041	4,172
5							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio 85.7 Mcf/bbl.
1.	.76	541	1.53	.924	A.P.I. Gravity of Liquid Hydrocarbons 54.0 @ 60 Deg.
2.	.78	539	1.52	.922	Specific Gravity Separator Gas .595
3.	.78	536	1.51	.922	Specific Gravity Flowing Fluid X X X X X
4.	.78	533	1.51	.922	Critical Pressure 672 P.S.I.A.
5.					Critical Temperature 354 °R

P _c 5958.2	P _c ² 35500.1		
NO.	P _t ²	P _w	P _w ²
1		4874.9	23763.7
2		4458.8	19880.9
3		3750.9	14069.3
4		2830.3	8010.6
5			

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 1.291$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.239$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 5.169$$

Absolute Open Flow 5,169 Mcfd @ 15.025	Angle of Slope θ 50	Slope, n .839
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Remarks: **6 Bbls of 54.0 (API) Condensate**

Approved By Commission:	Conducted By: Tom Hansen Company	Calculated By: Richard Turner	Checked By: Roy K. Valla
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