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See Rule 401 & Rule 1122

State of New Mexico
Energy, Minerals and Natural Resources Department

Form C-122
Revised 4-1-91

OIL CONSERVATION DIVISION

P.O. Box 2088
Santa Fe, New Mexico 87504-2088

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator TEXACO EXPLORATION					Lease or Unit Name BAKER B				
Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 10-14-96		Well No. 16		
Completion Date 7-9-96		Total Depth 6600		Plug Back TD 5800		Elevation		Unit Ltr. Sec. TYP - Rge. N 10-22S-37E	
Csg. Size 5 1/2	Wt. 15.5	d 4.950	Set At 6600	Perforations: From: 5424 To: 5552			County LEA		
Tbg. Size 2-3/8	Wt. 4.7#	d 1.995	Set At 5559	Perforations: From: To:			Pool		
Type Well - Single - Bradenhead - G.G. or G.O. Multiple single					Packer Set At none		Formation Blincry E		
Producing Thru TBG		Reservoir Temp. °F 114		Mean Annual Temp. °F 60		Baro. Press - P _a 13.2		Connection PIPELINE	
L 5424	H 5424	Gg .695	% CO ₂ .364	% N ₂ 2.882	% H ₂ S	Prover	Meter Run 3.068	Taps FLG.	

FLOW DATA					TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI						304				
1.					66.8	290				1 hr.
2.					69.5	240				1 hr.
3.					70.3	219				1.25hr
4.					72.0	165				1 hr.
5.										

RATE OF FLOW CALCULATIONS							
NO.	COEFFICIENT (24 HOUR)		Pressure P _m	Flow Temp. Factor Ft	Gravity Factor Fg	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.							380
2.	TAKEN FROM TOTAL FLOW METER						555
3.							791
4.							881
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P. I Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.		526.8			DRY	DRY	.695	DRY	*677	385
2.		529.5						XXXXXX		
3.		530.3								
4.		532.0								
5.										

P_c 317.2 P_e 100.6

NO.	P _i ²	P _w	P _w ²	P _c ² - P _w ²
1.	91.9	308.1	95.0	5.7
2.	64.1	265.8	70.6	30.0
3.	53.9	259.2	67.2	33.4
4.	31.8	220.0	48.4	57.2
5.				

1) $\frac{P_c^2}{P_c^2 - P_w^2} = 17.777$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1,602$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 4.216$

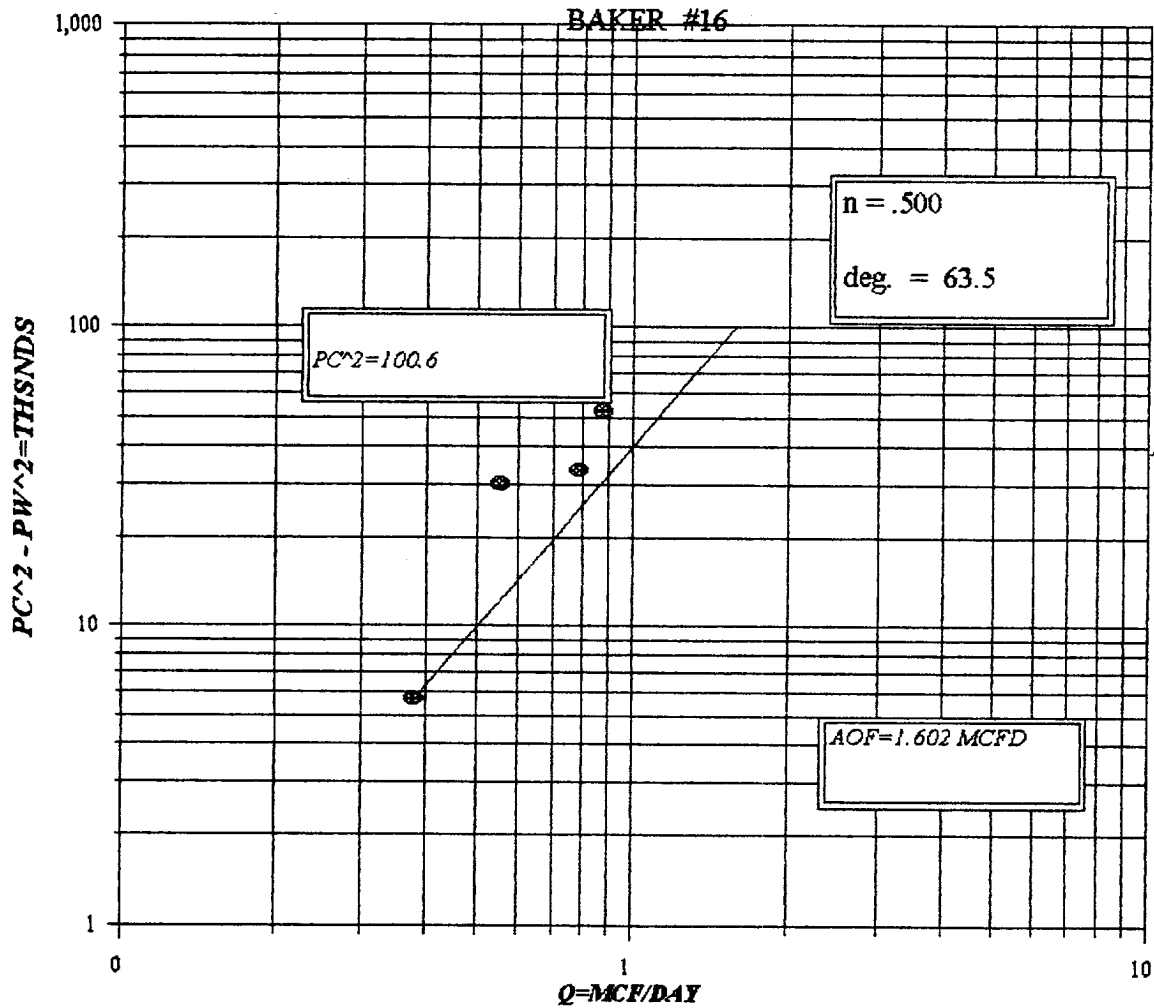
Absolute Open Flow 1,602 Mcfd @ 15.025	Angle of Slope Θ 63.5	Slope, n .500
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Remarks: ***CORRECTED TO 2% N₂**

Approved By Division	Conducted By: PRO WELL TESTER	Calculated By: KS	Checked By:
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TEXACO E & P

BAKER #16



0	COMPANY : TEXACO E & P				LEASE : BAKER 8				WELL NO. : 16				Pc = 317.2	Pc2 = 100.6	*
	UNIT : N				SECTION : 10				TOWNSHIP : 22						*
	L : 5424		H : 5424		L/H : 1		G/GMIX : 0.695		DATE : 10-14-96				Pt2 = 91.9	Pw = 308.1	*
	%CO2 : 0.364		%N2 : 2.882		H2S :				RANGE : 37				64.1	265.8	*
	d : 1.995		Fr : 0.018231		GH : 3769.7								53.9	259.2	*
													31.8	220.0	*
															*
	VOL 1 : 380		PSIA 1 : 303.2		RESV.TEMP 114.0				Pc2-Pw2= 5.7				Pw2 = 95.0		*
	VOL 2 : 555		PSIA 2 : 253.2						30.0				70.6		*
	VOL 3 : 791		PSIA 3 : 232.2		SHUT-IN PR= 317.2				33.4				67.2		*
	VOL 4 : 881		PSIA 4 : 178.2						52.2				48.4		*
															*
					PCR : 677				n = 0.500						*
					TCR : 385										*
									Pc2/(Pc2-Pw2) = 17.777						*
									3.355						*
									3.011						*
									1.927						*
															*
1	QM	0.380	0.380	0.555	0.555	0.791	0.791	0.881	0.881						*
2	TW	534	534	534	534	534	534	534	534	[Pc2/Pc2-Pw2]n = 4.216					*
3	Ts	574.0	574.0	574.0	574.0	574.0	574.0	574.0	574.0	1.832					*
4	T	554.0	554.0	554.0	554.0	554.0	554.0	554.0	554.0	1.735					*
	PR (est)	0.45		0.37		0.34		0.26		1.388					*
5	Z(est)	0.926	0.922	0.934	0.930	0.937	0.932	0.946	0.940						*
6	TZ	512.8	510.5	517.4	515.0	519.3	516.3	524.2	520.9	AOF= Q 1.602					*
7	GH/TZ	7.351	7.384	7.286	7.319	7.259	7.301	7.191	7.238	1.017					*
8	eS	1.317	1.319	1.314	1.316	1.313	1.315	1.310	1.312	1.372					*
9	l-e-S	0.241	0.242	0.239	0.240	0.238	0.239	0.236	0.238	1.223					*
10	Pt	303.2	303.2	253.2	253.2	232.2	232.2	178.2	178.2						*
11	Pt2 /1000	91.9	91.9	64.1	64.1	53.9	53.9	31.8	31.8						*
12	Fr	0.018231	0.018231	0.018231	0.018231	0.018231	0.018231	0.018231	0.018231						*
13	Fc=FrTZ	9.350	9.308	9.433	9.390	9.467	9.413	9.557	9.496						*
14	FcQm	3.55	3.54	5.24	5.21	7.49	7.45	8.42	8.37						*
15	L/H(FcQm)	12.6	12.5	27.4	27.2	56.1	55.4	70.9	70.0						*
16	Fw	3.041100	3.025703	6.552175	6.518618	13.36479	13.27878	16.75647	16.635184						*
17	Pw2	95.0	95.0	70.7	70.6	67.3	67.2	48.5	48.4						*
18	Ps2	125.1	125.2	92.9	92.9	88.3	88.4	63.5	63.5						*
19	Ps	353.7	353.9	304.7	304.9	297.2	297.2	252.0	252.0						*
20	P	328.5	328.6	279.0	279.0	264.7	264.7	215.1	215.1						*
21	Pr	0.49	0.49	0.41	0.41	0.39	0.39	0.32	0.32						*
22	Tr	1.44	1.44	1.44	1.44	1.44	1.44	1.44	1.44						*
23	Z	0.922	0.922	0.930	0.930	0.932	0.932	0.940	0.940	FORM C122-D					*

TEXACO E & P INC.
EUNICE G. P. LAB
P. O. BOX 1929
EUNICE, N.M.
PHONE 505-394-2516

SAMPLE SERIAL NO. 9456
DATE SAMPLE SECURED: 08-16-96
DATE SAMPLE ANALYZED: 08-19-96

SAMPLE OF: BAKER B-16 STA.#11-021-3386
SAMPLE FROM: T. E. P. I.

ANALYSIS REQUESTED BY: C. R. ADKISON
ANALYSIS COMPLETED BY: R. WOODELL

COMPONENT	MOL %	GPM	WT. %
CARBON DIOXIDE	0.364		0.793
NITROGEN	2.882		3.999
METHANE	80.985		64.352
ETHANE	9.119	2.426	13.582
PROPANE	4.114	1.127	8.985
ISO-BUTANE	0.470	0.153	1.353
N-BUTANE	1.157	0.363	3.331
ISO-PENTANE	0.264	0.096	0.943
N-PENTANE	0.290	0.104	1.036
HEXANE HEAVIER	0.355	0.146	1.626
TOTAL	100.000	4.415	100.000

CALCULATED PHYSICAL PROPERTIES @ 14.65 psia & 60 F

sp gr. air = 1	0.695	BTU wet basis	1151.733
Cp	0.496	BTU dry basis	1172.128
mol. wt.	20.190	critical temp. R	384.112
acentric factor	0.031	critical press.	661.312
Cp/cv	1.247	26 # GPM	0.524

CC: C. R. ADKISON
M. ALEXANDER
W. BROACH
R. A. DUNCAN
O. BRADLEY
LAB FILE