NEW MEXICO OIL CONSERVATION COMMSSION

MULTIPOINT AND E POINT BACK PRESSURE TEST F(GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special				Test Date: 5-31-79	
Company: AMOCO PRODUCTION COMPANY			Connection: LLANO GAS COMPANY		
Pool: UNDESIGNATED			Formation: ~~MORROW~~ ATOKA		Unit
Completion Date: 1 28 79	Total Depth: 15808.		Plug Back TD: 14815.	Elevation: 3679.	Farm or Lease Name: FEDERAL H
Csg. Size: 5.000 / Wt.: 18.0 / d: 4.276	Set At: 15807.		Perforations: From 14725. To 14742.		Well No.: 1
Tbg. Size: 2.375 / Wt.: 4.7 / d: 1.995	Set At: 14637.		Perforations: From 0. To 0.		Unit: L / Sec.: 26 / Twp.: 23S / Rge.: 33E
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: SINGLE			Packer Set At: 11806.		County: LEA
Producing Thru: TUBING	Reservoir Temp. °F: 224. @ 14733.	Mean Annual Temp. °F: 60.0	Baro. Press. – P_a: 13.2		State: NEW MEXICO

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
14733.	14733.	0.597	0.35	1.38	0.	0.	3.1	FLANGE

	FLOW DATA				TUBING DATA		CASING DATA		
NO.	Prover Line Size X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI					2290.	66.			46.0
1.	3.09 x 2.000	420.	1.8	50.	1980.	67.	0.	0.	1.0
2.	3.09 x 2.000	420.	3.8	55.	1755.	70.	0.	0.	1.0
3.	3.09 x 2.000	420.	5.6	56.	1557.	70.	0.	0.	1.0
4.	3.09 x 2.000	420.	6.9	57.	1377.	70.	0.	0.	1.0
5.									

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	21.26	27.92	433.2	1.0098	1.2937	1.0398	807.
2.	21.26	40.57	433.2	1.0048	1.2937	1.0384	1165.
3.	21.26	49.25	433.2	1.0039	1.2937	1.0381	1412.
4.	21.26	54.67	433.2	1.0029	1.2937	1.0378	1565.
5.							

NO.	P_r	Temp. °R	T_r	Z
1.	0.64	510.	1.44	0.925
2.	0.64	515.	1.46	0.927
3.	0.64	516.	1.46	0.928
4.	0.64	517.	1.46	0.928
5.				

Gas Liquid Hydrocarbon Ratio 0. Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons 0. Deg.
Specific Gravity Separator Gas 0.597 XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX 0.597
Critical Pressure 672. P.S.I.A. 672. P.S.I.A.
Critical Temperature 353. R 353. R

P_c 2297.3 P_c^2 5278.

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1	3973.	1990.	3961.	1317.
2	3127.	1766.	3120.	2157.
3	2466.	1574.	2478.	2800.
4	1933.	1400.	1959.	3318.
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.5904$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.3929$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 2181.$

Absolute Open Flow 2181. Mcfd @ 15.025 Angle of Slope θ 54.5 Slope, n 0.714

Remarks:

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
John W. Runyan	John West Engr	C.C. Weaver	W.D. Magness

3 - NMOCD
1 - Hou
1 - Susp
1 - WDM
1 - DLB
1 - Southland Royalty Co.