

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 11/13/80	
Company NATOMAS NORTH AMERIA, INC.				Connection El Paso	
Pool Antelope Ridge				Formation Atoka	
Completion Date 10/15/80		Total Depth 13,595'		Plug Back TD 13,511'	
				Elevation 3375'	
Casing Size 7-5/8"		Wt. 39#		Set At 13,595'	
Perforations: From 13,214' To 13,222'				Well No. 1	
Tubing Size 2-7/8"		Wt. 6.5#		Set At 12,948'	
Perforations: From 13,260' To 13,262'				Unit K	
				Sec. 14	
				Twp. 23S	
				Range 34E	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Dual				Packer Set At 12,900'	
Producing Thru Tbg				State New Mexico	
Reservoir Temp. °F 170° 12,093'		Mean Annual Temp. °F 60°		Baro. Press. - P _a 13.20	
L 12,093'		H 12,093'		G _g .650	
				% CO ₂	
				% N ₂	
				% H ₂ S	
				Prover	
				Meter Run 4.0	
				Taps Flange	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							5388	60			72 hrs
1.	4.03		2.5	564	6.2	103	5122	64			1 hr
2.	4.03		2.5	580	9.0	72	5001	76			1 hr
3.	4.03		2.5	611	23.0	50	4325	80			1 hr
4.	4.03		2.5	611	36.0	30	4160	80			1 hr
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{sp}	Rate of Flow Q, Mscf/d
1	32.64	60.08	577.6	.9611	1.2403	1.0449	2443
2	32.64	73.05	592.9	.9887	1.2403	1.0575	3092
3	32.64	119.91	624.1	1.0098	1.2403	1.0719	5254
4	32.64	149.89	624.1	1.0302	1.2403	1.0837	6774
5							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mscf/bbl.
1	.86	563	1.50	.916	A.P.I. Gravity of Liquid Hydrocarbon _____ 53.8 _____ Deg.
2	.88	532	1.42	.894	Specific Gravity Separator Gas _____ .650 _____ X X X X X X X X
3	.93	510	1.36	.870	Specific Gravity Flowing Fluid _____ X X X X X _____ .650 _____
4	.93	490	1.31	.851	Critical Pressure _____ 670 _____ P.S.I.A. _____ 670 _____ P.S.I.A.
5					Critical Temperature _____ 374 _____ R _____ 374 _____ R

NO.	P _c	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$
1	5401.2	29173			2.5538	1.9536
1		5142	26440	2733		
2		5009	25086	4087		
3		4352	18936	10237		
4		4213	17749			
5						

Absolute Open Flow _____ 13,234 _____ Mscf @ 15.025				Angle of Slope θ _____ 54.5 _____	
Slope, n _____ .714 _____					
Remarks: _____					

Approved By Division Jerry Sexton	Conducted By: Kenneth Brewster	Calculated By: Garrett Systems	Checked By: Art Oneal
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