



Correction MULTIPoint AND ONE POINT BACK PRESSURE TEST FOR GAS

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 1-20-81	
Company Estoril Producing Corp.		Connection To Atmosphere	
Pool Antelope Ridge		Unit Strawn	
Completion Date	Total Depth 13,640	Plug Back TD 12,882	Elevation 3436 K.B.
Farm or Lease Name Curry Federal		Well No. 1	
Chq. Size 5 1/2 liner	Wt. 23# 29.7	Set At 4.670	Perforations: 11,363-13,409 From 12,048 To 12,197
Tbg. Size 3 1/2	Wt. 10.2#	Set At 2.992	Perforations: From Open ended To
Type Well - Single - Brodenhead - G.G. or G.O. Multiple Single		Packer Set At 11,407	County Lea
Producing Thru Tbg.	Reservoir Temp. °F 195 @ 12,222	Mean Annual Temp. °F 600	Buro. Press. - P _a 13.2
State New Mexico		State	
L 12,222	H 12,222	G _g .6335	% CO ₂ .228
% N ₂ 1,040	% H ₂ S	Prover	Meter Run 4"
Flg.		Flg.	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI		X					6477		Pkr.	Choke	72 hours
1.	4"	X	1.750	900	65"	65 ⁰	5285			15/64	12.50
2.	4"	X	1.750	900	49"	70 ⁰	5485			12/64	0.50
3.	4"	X	1.750	900	38"	76 ⁰	5638			10/64	0.50
4.	4"	X	1.750	900	25"	77 ⁰	5800			8/64	0.75
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	14.93	243.63	913.2	.9952	1.256	1.088	4947
2	14.93	211.53	913.2	.9905	1.256	1.085	4263
3	14.93	186.28	913.2	.9850	1.256	1.080	3716
4	14.93	151.10	913.2	.9840	1.256	1.080	3011
5							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.G. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1	1.36	525	1.43	.845	59.0	60 ⁰	.6335	X X X X X X X X	670	699
2	1.36	530	1.44	.850				X X X X X		388
3	1.36	536	1.46	.857						
4	1.36	537	1.46	.857						
5										

NO.	P _t	P _w	P _w ²	P _t ² - P _w ²	(1) $\frac{P_t^2}{P_t^2 - P_w^2}$	(2) $\left[\frac{P_t^2}{P_t^2 - P_w^2} \right]^n$
1	6490.2	42,122.7	5306.8	28,162	3.0173	2.6425
2			5505	30301.		
3			5655	31979		
4			5817	33837		
5						

Absolute Open Flow	13,072	Hold @ 15.025	Angle of Slope	48° 39'	Slope, n	.8799
Remarks:						
Approved By Division						
Conducted By:		W.S.		Calculated By:		M.K.
				Checked By:		M.K.

RECEIVED

MAY 28 '81

OIL CONSERVATION DIV.