

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 3-18-86		Lease Designation 19143	
Company Diamond Shamrock Exploration Co.				Connection Negotiating Contract				
Pool Antelope Ridge				Formation Atoka				Unit G
Completion Date 3-18-86		Total Depth 13552		Plug Back TD 12,408		Elevation 3389 GR		Farm or Lease Name Federal
Ceq. Size 5 1/2 Liner	Wt. 20#	d 4.778	Set At 11418 B-12408	Perforations: From 12,084 To 12,112		Well No. #1		
Thq. Size 2 7/8	Wt. 6.5	d 2.441	Set At 11946	Perforations: From 12,084 To 12,112		Unit Sec. Twp. Rge. G 3 23S 34E		
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single Gas					Packer Set At 11,946		County Lea	
Producing Thru 2 7/8" tubing		Reservoir Temp. °F 175@ 12098		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2		State New Mexico
L 12,098	H 12,098	Gg .668	% CO ₂ .25	% N ₂ 1.12	% H ₂ S --	Prover	Meter Run X	Taps F

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							4913		Packer		+ 72 hrs
1.	4 x 2.250			150	6.0	86	4834	70			1 hr.
2.	4 x 2.250			300	15.0	85	4716	70			1 hr.
3.	4 x 2.250			450	37.0	71	4657	73			1 hr.
4.	4 x 2.250			900	68.0	63	4284	75			1 hr. 15 min.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	25.99	30	150	.9759	.947736	1.01375	731
2	25.99	67	300	.976795	.947736	1.02818	1659
3	25.99	129	450	.989588	.947736	1.0474	3294
4	25.99	247	900	.997128	.947736	1.1065	6723
5							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1	3.81	520	1.60	1.021	73,200/1	56.7	.668	X X X X X X X X	669	322
2	3.72	520	1.60	1.016				X X X X X		
3	3.67	520	1.60	1.013						
4	3.38	520	1.61	.995						
5										

$P_c = 6778$ $P_c^2 = 45941$					$(1) \frac{P_c^2}{P_c^2 - P_w^2} = \frac{45941}{45941 - 6754} = \frac{45941}{39187} = 1.172$		$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \left[1.172 \right]^n = 1.172^n$	
NO.	P _i ²	P _w	P _w ²	P _c ² - P _w ²	$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.172^n$			
1	23495	6754	45617	324				
2	22365	6710	45024	917				
3	21811	6602	43586	2355				
4	18466	6336	40145	5796				
5								

Absolute Open Flow 34,000 Mcfd @ 15.025		Angle of Slope θ 53°		Slope, n .754	
Remarks: 45 Bbls of condensate was produced during the test.					
Approved By Division		Conducted By: Greg McMurry		Checked By: Scott Moss	

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MAR 25 1986
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HOBBS OFFICE

Company Diamond Shamrock Exploration Co.

Well Name Federal

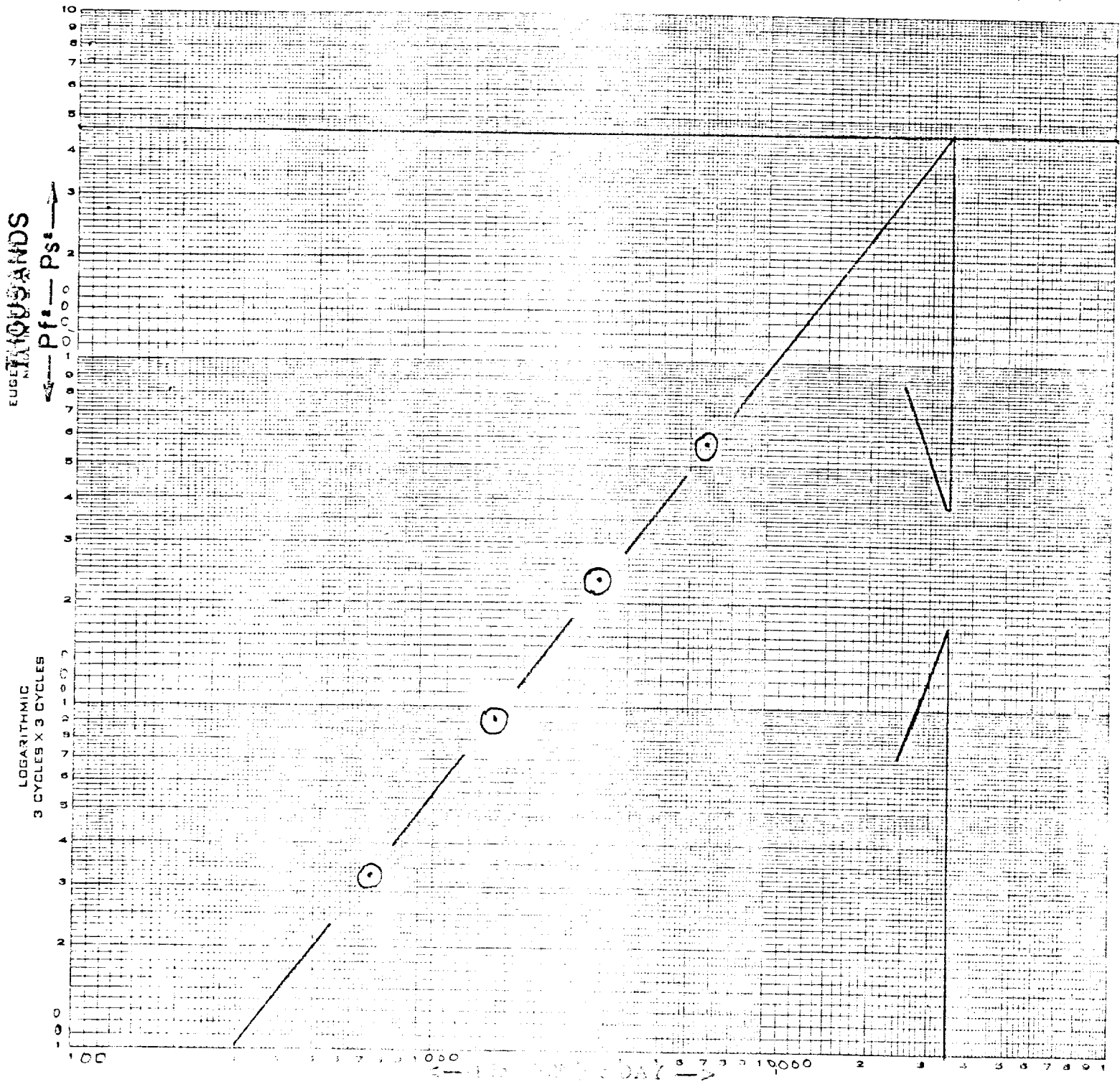
Well No. 1

Date 3/19/86

Angle of Curve 53° Slope of Curve n 1.754

Absolute Open Flow 34,000 MCF/Day

GAS WELL
BACK PRESSURE CURVE



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