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See Rule 401 & Rule 1122

State of New Mexico
Energy, Minerals and Natural Resources Department
OIL CONSERVATION DIVISION
P.O. Box 2088
Santa Fe, New Mexico 87504-2088

Form C-122
Revised 4-1-1991

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator Endeavor Energy Resources LP						Lease or Unit Name CURRY STATE			
Test Type ☒ Initial ☐ Annual ☐ Special						Test Date 10-30-01		Well No. 4	
Completion Date 10-12-01		Total Depth 13375		Plug Back TD 13120		Elevation 3402		Unit Ltr - Sec - TWP - Rge. S22T23SR34ENMPM	
Csg. Size 4.500	Wt. 13.500	d 3.925	Set At 13375	Perforation: From 13041 To 13051		County LEA			
Tbg. Size 2.875	Wt. 6.500	d 2.446	Set At 12927	Perforation: From To		Pool ANTELOPE RIDGE			
Type Well-Single-Bradenhead-G.G. or G.O. Multiple SINGLE						Packer Set At 12927		Formation MORROW	
Producing Thru TUBING		Reservoir Temp.F		Mean Annual Temp.F 70		Baro. Pressure 13.20		Connection	
L 13375	H 13375	Gg .618	% CO ₂ .34	% N ₂ .30	% H ₂ S	Prover METER		Meter Run 6.063	Taps FLANGE

Flow Data					Tubing Data		Casing Data		SIP/Flow Duration (HRS.)
No.	(Prover) Line Size/Orifice Size	Press. PSIG	Diff. h _w	Temp. F	Press. PSIG	Temp. F	Press. PSIG	Temp. F	
Shut-in Pressure					6561	71		71	100
1.	6.06 x 1.38	203.00	2.60	63	5860	71		71	1
2.	6.06 x 1.38	203.00	9.00	72	4868	71		71	1
3.	6.06 x 1.38	203.00	21.00	81	4048	70		71	1
4.	6.06 x 1.38	203.00	36.00	82	3108	70		71	1

RATE OF FLOW CALCULATIONS

No.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. FACTOR F _t	Gravity FACTOR F _g	Super Compress. FACTOR F _{pv}	Rate of Flow (Q) MCFD
1.	8.973	23.709	216.2	.9971	1.2721	1.0182	274.7
2.	8.973	44.111	216.2	.9887	1.2721	1.0172	506.3
3.	8.973	67.381	216.2	.9804	1.2721	1.0162	766.2
4.	8.973	88.222	216.2	.9795	1.2721	1.0161	1002.2

No.	P _r	TEMP.	T _r	Z
1.	.322	523	1.450	.9646
2.	.322	532	1.475	.9665
3.	.322	541	1.500	.9684
4.	.322	542	1.503	.9685

Gas-Liquid Hydrocarbon Ratio		Mcf/bbl
API Gravity of Liquid Hydrocarbons		
Specific Gravity Separator Gas	.618	
Specific Gravity Flowing Fluid		.618
Critical Pressure	672 PSIA	672 PSIA
Critical Temperature	360 R	360 R

$P_C = 6574.2$ $P_C^2 = 43220.1$

No.	P _w	P _w ²	P _C ² - P _w ²
1.	5873.4	34496	8723.471
2.	4881.8	23831	*****
3.	4062.5	16504	*****
4.	3123.7	9757	*****

(1) $\frac{P_C^2}{P_C^2 - P_W^2} = \frac{1.292}{\left[\frac{P_C^2}{P_C^2 - P_W^2} \right]^n} = \frac{1.281}{\left[\frac{P_C^2}{P_C^2 - P_W^2} \right]^n}$

AOF = Q $\left[\frac{P_C^2}{P_C^2 - P_W^2} \right]^n = \frac{1283}{\left[\frac{P_C^2}{P_C^2 - P_W^2} \right]^n}$

Absolute Open Flow		1283	Mcf/d @ 15.025	Angle of Slope -	46.0	Slope, n	.967
Remarks							
Approved By Division:		Conducted By: L RACKLEY		Calculated By: BPT System		Checked By:	