appropriate district office
See Rule 401 & Rule 1122

Revised 4-1-91

OIL CONSERVATION DIVISIC

P.O. Box 2088
Santa Fe, New Mexico 87504-2088

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator: KAISER-FRANCIS Oil Company							Lease or Unit Name: BELL LAKE UNIT 1		
Type Test: [X] Initial [ ] Annual [ ] Special							Test Date: 4/19/97	Well No.: 4	
Completion Date: 4/17/97		Total Depth: 15566		Plug Back TD: 13320			Elevation: 3615 DF	Unit Ltr. - Sec. - TWP - Rge.: F 6-24S-34E	
Csg. Size: liner 7"/5-1/2	Wt.: 32/15	d: 6.094 / 4.892	Set At: 14561 / 15566	Perforations: From: 13261 To: 13294				County: LEA	
Tbg. Size: 2-7/8	Wt.: 6.5	d: 2.44	Set At: 13069	Perforations: From: - To: -				Pool: Bell Lake Morrow South	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple: single				Packer Set At: 13037				Formation: MORROW	
Producing Thru: TBG	Reservoir Temp. °F: 206.6	Mean Annual Temp. °F: 60		Baro. Press - P_a: 13.2				Connection: AIR	
L: 13261	H: 13261	Gg: .580	% CO_2: .49	% N_2: .32	% H_2S:	Prover: -0-	Meter Run: 4.026	Taps: FLG	

	FLOW DATA				TUBING DATA		CASING DATA		
NO.	Prover Line Size X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI					4000		PKR.		
1.	4.026 X 1.750	500	3	100°	3700	76	"		60 min
2.	4.026 X 1.750	550	8	100°	3450	76	"		60 min
3.	4.026 X 1.750	550	9	86°	3325	75	"		60 min
4.	4.026 X 1.750	550	18	72°	3125	76	"		60 min
5.									

RATE OF FLOW CALCULATIONS

NO.	COEFFICIENT (24 HOUR)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg.	Super Compress. Factor, F pv.	Rate of Flow Q, Mcfd
1.	14.93	39.23	513.2	.9636	1.313	1.033	765
2.	14.93	67.12	563.2	.9636	1.313	1.033	1309
3.	14.93	71.19	563.2	.9759	1.313	1.036	1410
4.	14.93	100.68	563.2	.9887	1.313	1.039	2027
5.							

NO.	P_r	Temp. °R	T_r	Z
1.	.82	560	1.61	.938
2.	.82	560	1.61	.938
3.	.80	546	1.57	.932
4.	.78	532	1.53	.927
5.				

Gas Liquid Hydrocarbon Ratio: N/A Mcf/bbl.
A.P. I. Gravity of Liquid Hydrocarbons: N/A Deg.
Specific Gravity Separator Gas: .580 XXXXXXXXX
Specific Gravity Flowing Fluid: N/A XXXXX
Critical Pressure: 675 P.S.I.A. P.S.I.A.
Critical Temperature: 346 R R

P_c 4013.2 P_c^2 16105.7

NO.	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1.		3714.3	13796.3	2309.5
2.		3466.7	12018.0	4087.8
3.		3342.4	11171.4	4934.4
4.		3147.2	9904.9	6200.8
5.				

1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.597$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 2.575$

$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 5.220$

Absolute Open Flow 5.220 Mcfd @ 15.025 | Angle of Slope θ 45.24 | Slope, n .991

Remarks: NO FLUID MADE DURING TEST

Approved By Division	Conducted By:	Calculated By:	Checked By:
	PRO WELL TESTER	MB	BM

0 COMPANY :KAISER FRANSIS LEASE :B''LAKE 4 WELL NO. : 1

UNIT : SECTION : TOWNSHIP :

L : 13261 H : 13261 L/H : 1 G/GMIX : 0.580

%CO2 : 0.49 %N2 : 0.32 H2S : DATE :4/19/97

d : 2.44 Fr :0.010774 GH : 7691.4 RANGE :

VOL 1 : 765 PSIA 1 : 3713.2 RESV.TEMP 206.6

VOL 2 : 1309 PSIA 2 : 3463.2

VOL 3 : 1410 PSIA 3 : 3338.2 SHUT-IN PR= 4013.2

VOL 4 : 2027 PSIA 4 : 3138.2

PCR : 675

TCR : 346

LINE	RATE 1		RATE 2		RATE 3		RATE 4	
	1ST	2ND	1ST	2ND	1ST	2ND	1ST	2ND
1 QM	0.765	0.765	1.309	1.309	1.410	1.410	2.027	2.027
2 TW	534	534	534	534	534	534	534	534
3 Ts	666.6	666.6	666.6	666.6	666.6	666.6	666.6	666.6
4 T	600.3	600.3	600.3	600.3	600.3	600.3	600.3	600.3
PR (est)	5.50		5.13		4.95		4.65	
5 Z(est)	0.891	0.923	0.880	0.907	0.875	0.899	0.867	0.888
6 TZ	535.0	554.1	528.1	544.3	525.0	539.8	520.7	533.0
7 GH/TZ	14.376	13.880	14.565	14.129	14.650	14.249	14.772	14.430
8 eS	1.714	1.683	1.727	1.699	1.732	1.706	1.740	1.718
9 1-e-S	0.417	0.406	0.421	0.411	0.423	0.414	0.425	0.418
10 Pt	3713.2	3713.2	3463.2	3463.2	3338.2	3338.2	3138.2	3138.2
11 Pt2 /1000	13787.9	13787.9	11993.8	11993.8	11143.6	11143.6	9848.3	9848.3
12 Fr	0.010774	0.010774	0.010774	0.010774	0.010774	0.010774	0.010774	0.0107746
13 Fc=FrTZ	5.765	5.970	5.690	5.865	5.657	5.816	5.610	5.743
14 FcQm	4.41	4.57	7.45	7.68	7.98	8.20	11.37	11.64
15 L/H(FcQm)	19.4	20.9	55.5	58.9	63.6	67.2	129.3	135.5
16 Fw	8.104120	8.465119	23.34593	24.24434	26.89046	27.83603	55.00041	56.633502
17 Pw2	13796.0	13796.3	12017.1	12018.0	11170.5	11171.4	9903.3	9904.9
18 Ps2	23652.8	23217.7	20749.1	20414.8	19349.2	19062.3	17232.8	17016.0
19 Ps	4863.4	4818.5	4555.1	4518.3	4398.8	4366.0	4151.2	4125.0
20 P	4288.3	4265.8	4009.2	3990.7	3868.5	3852.1	3644.7	3631.6
21 Pr	6.35	6.32	5.94	5.91	5.73	5.71	5.40	5.38
22 Tr	1.73	1.73	1.73	1.73	1.73	1.73	1.73	1.73
23 Z	0.923	0.922	0.907	0.906	0.899	0.898	0.888	0.887

Pc = 4013.2 Pc2 = 16105.8

Pt2 = ******* Pw = 3714.3

******* 3466.7

******* 3342.4

9848.3 3147.2

Pc2-Pw2= 2309.5 Pw2 = 13796.3

4087.8 12018.0

4934.4 11171.4

6200.8 9904.9

n = 0.991

Pc2/(Pc2-Pw2) = 6.974

3.940

3.264

2.597

[Pc2/Pc2-Pw2]n = 6.853

3.892

3.229

2.575

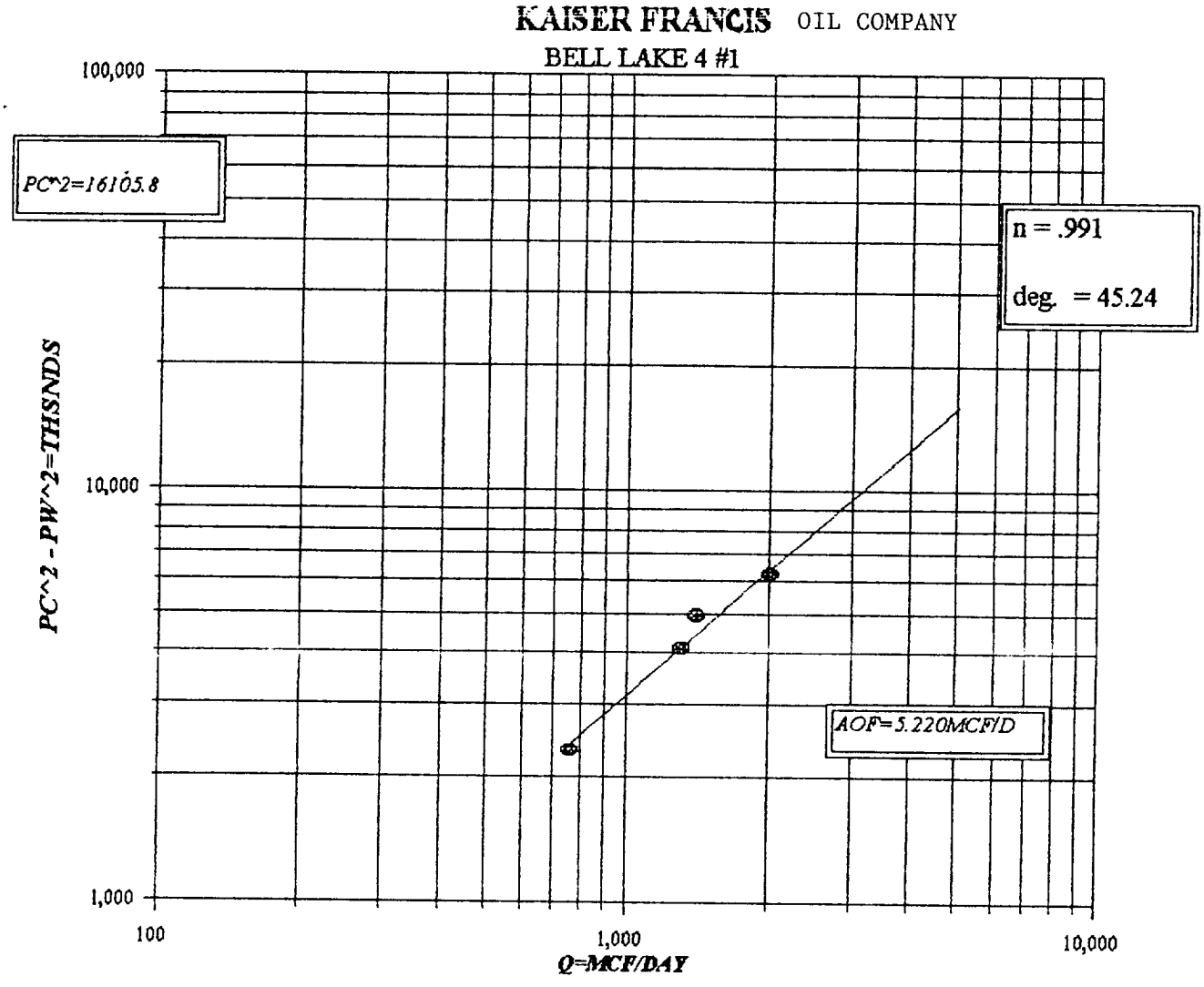
AOF= Q 5.243

5.094

4.554

5.220

FORM C122-D



Attachment to C-122
Test date: 4/19/97