NE MEXICO OIL CONSERVATION COMMISSION

MULTIPOINT A ONE POINT BACK PRESSURE TEST OR GAS WELL

Form C-122
Revised 9-1-65

Type Test: ☒ Initial ☐ Annual ☐ Special			Test Date: 6-27-73	
Company: Continental Oil Co.	Connection: Trans western Pipeline Company			
Pool	Formation: Atoka			Unit: Bell Lake
Completion Date: 6-28-73	Total Depth: 15,566'	Plug Back TD: 14,000'	Elevation: 3615' d.F.	Farm or Lease Name: Bell Lake unit
Csg. Size: 7" / Wt.: 32# / d / Set At: 14,561'	Perforations: From 12,450 To 12,486'			Well No.: 4
Tbg. Size: 2 3/8" / Wt. / d / Set At: 12,028'	Perforations: From To			Unit: F / Sec.: 6 / Twp.: 24S / Rge.: 34E
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single		Packer Set At: 12000'		County: Lea
Producing Thru: Tbg	Reservoir Temp. °F: @ 176°	Mean Annual Temp. °F	Baro. Press. – P_a: 13.2	State: New Mexico

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
12028	12028	0.582					4"	Flange

NO.	FLOW DATA: Prover Line Size X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	TUBING DATA: Press. p.s.i.g.	Temp. °F	CASING DATA: Press. p.s.i.g.	Temp. °F	Duration of Flow
SI	4" x 2"				6906				SI
1.	4" x 2"	945	11.5	102°	6660	89°			3
2.	4" x 2"	945	28.8	92°	6625	93°			3
3.	4" x 2"	960	53.0	82°	6455	98°			3
4.	4" x 2"	990	88.0	75°	6150	105°			3
5.	4" x 2"	978	43.0	91°	6625	103°			17

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	19.81	104.98	958.2	0.9628	1.311	1.058	2,780
2	19.81	166.60	958.2	0.9706	1.311	1.060	4,450
3	19.81	228.30	983.2	0.9795	1.311	1.068	6,202
4	19.81	297.10	1003.2	0.9859	1.311	1.075	8,180
5	19.81	206.50	991.2	0.9715	1.311	1.062	5,533

NO.	P_t	Temp. °R	T_r	Z
1	1.425	562	1.606	0.894
2	1.425	552	1.580	0.890
3	1.463	542	1.549	0.877
4	1.493	535	1.529	0.866
5	1.475	551	1.574	0.887

Gas Liquid Hydrocarbon Ratio 300.70 Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons ____ Deg.
Specific Gravity Separator Gas 0.582 XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX 0.6868
Critical Pressure 672 P.S.I.A. 669 P.S.I.A.
Critical Temperature 350 R 389 R

P_c 8573 P_c^2 73,496 +L.J.

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		8278	68,525	4,971
2		8223	67,617	5,879
3		8106	65,707	7,789
4		7959	63,345	10,151
5		8223	67,617	5,879

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 12.50$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^{n/1} = 12.50$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 69,000$ mcfpd

Absolute Open Flow 69,000 Mcfd @ 15.025 Angle of Slope θ 45° Slope, n 1

Remarks:

Approved By Commission:	Conducted By: W.E. Tucker N.S. Mendoza	Calculated By: N.S. Mendoza	Checked By: