

## NEW MEXICO OIL CONSERVATION COMMISSION

Form C-122

## MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Revised 12-1-55

Pool Jalmat Formation Y - S.R. County Lea  
Initial Annual Special X Date of Test 3-27-59 to 4-2-59  
Company Amerada Petroleum Corporation Lease State LM"T" Well No. 2  
Unit F Sec. 21 36 Twp. 23-S Rge. 36-E Purchaser Permian Basin Pipeline Co.  
Casing 5-1/2" Wt. 15.5# I.D. 4.950" Set at 3455' Perf. 2930' To 3430'  
Tubing 2-3/8" Wt. 4.7# I.D. 1.995" Set at 2926' Perf. Open End To   
Gas Pay: From 2930' To 3430' L 2926' xG 0.655 -GL 1917 Bar.Press. 13.2  
Producing Thru: Casing  Tubing X Type Well Single  
Date of Completion: 3-29-59 Packer None Single-Bradenhead-G. G. or G.O. Dual 84°  
Reservoir Temp. 84°

## OBSERVED DATA

Tested Through <del>(Prover)</del> (Choke) (Meter)						Type Taps		Pipe		
No.	Flow Data					Tubing Data		Casing Data		Duration of Flow Hr.
	<del>(Prover)</del> (Line) Size	<del>(Choke)</del> (Orifice) Size	Press. psig	Diff. h <sub>w</sub>	Temp. °F.	Press. psig	Temp. °F.	Press. psig	Temp. °F.	
SI						786.2	None	786.9	None	72.00
1.	4"	2.25	95.1	3.1	106	741.6	-	754.3	-	24.00
2.	4"	2.25	130.1	8.6	48	669.1	-	706.0	-	24.00
3.	4"	2.25	94.6	23.8	76	571.4	-	647.3	-	24.00
4.	4"	2.25	119.7	38.6	75	414.7	-	570.8	-	24.00
5.										

## FLOW CALCULATIONS

No.	Coefficient (24-Hour)	$\sqrt{h_w P_f}$	Pressure psia	Flow Temp. Factor F <sub>t</sub>	Gravity Factor F <sub>g</sub>	Compress. Factor F <sub>pv</sub>	Rate of Flow Q-MCFPD @ 15.025 psia
1.	40.58	18.33	108.4	0.9585	0.9571	1.007	686
2.	40.53	35.10	143.3	1.0117	0.9571	1.015	1398
3.	40.53	50.66	107.8	0.9850	0.9571	1.008	1951
4.	40.53	71.62	132.9	0.9859	0.9571	1.010	2766
5.							

## PRESSURE CALCULATIONS

Gas Liquid Hydrocarbon Ratio 276,600\* cf/bbl.  
Gravity of Liquid Hydrocarbons 24° (frac oil) deg.  
F<sub>c</sub> P<sub>w</sub> measured (1-e<sup>-s</sup>) 0.124  
Specific Gravity Separator Gas 0.655  
Specific Gravity Flowing Fluid -  
P<sub>c</sub> 800.1 P<sub>c</sub><sup>2</sup> 640.2

No.	P <sub>w</sub> P <sub>t</sub> (psia)	P <sub>t</sub> <sup>2</sup>	F <sub>c</sub> Q	(F <sub>c</sub> Q) <sup>2</sup>	(F <sub>c</sub> Q) <sup>2</sup> (1-e <sup>-s</sup> )	P <sub>w</sub> <sup>2</sup>	P <sub>c</sub> <sup>2</sup> -P <sub>w</sub> <sup>2</sup>	Cal. P <sub>w</sub>	P <sub>w</sub> P <sub>c</sub>
1.	767.5	-	-	-	-	589.1	51.1	-	0.959
2.	719.2	-	-	-	-	517.2	123.0	-	0.899
3.	660.5	-	-	-	-	436.3	203.9	-	0.826
4.	584.0	-	-	-	-	341.1	299.1	-	0.730
5.									

Absolute Potential: 4982 MCFPD; n .773  
COMPANY Amerada Petroleum Corporation  
ADDRESS Brewer "D" - Monument, New Mexico  
AGENT and TITLE R. E. Busch District Engineer Test by: R.L. West  
WITNESSED E.E. Shirley Permian Basin P.L. Co.  
COMPANY Amerada Petroleum Corporation

## REMARKS

\* Produced 1 bbl frac oil on 3rd flow rate and 10 bbls on 4th flow rate

This is corrected copy of a Special Test following workover on well.

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

$Q$  = Actual rate of flow at end of flow period at W. H. working pressure ( $P_w$ ).  
MCF/da. @ 15.025 psia and 60° F.

$P_c$  = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater.  
psia

$P_w$  = Static wellhead working pressure as determined at the end of flow period.  
(Casing if flowing thru tubing, tubing if flowing thru casing.) psia

$P_t$  = Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia

$P_f$  = Meter pressure, psia.

$h_w$  = Differential meter pressure, inches water.

$F_g$  = Gravity correction factor.

$F_t$  = Flowing temperature correction factor.

$F_{pv}$  = Supercompressability factor.

$n$  = Slope of back pressure curve.

Note: If  $P_w$  cannot be taken because of manner of completion or condition of well, then  $P_w$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_t$ .