

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 5-5-77	
Company GULF ENERGY & MINERALS		Connection AIR	
Well TEAGUE-DEVONIAN NORTH		Unit	
Completion Date 4-29-77	Total Depth 8015	Plug Back TD 8015	Elevation 1 Gr.
Form or Lease Name LA MUNYON		Well No. 11	
Case Size 7.00"	Wt. 24.00#	d 6.336"	Set At 8015
Perforations: From 7373 To 7427	Perforations: From To		Unit Sec. Twp. Rgt.
Case Size 2.875 EUE	Wt. 6.50#	d 2.441"	Set At 7318
Type Well - Single - Graduated - G.G. or G.O. Multiple		Packer Set At 7318	
Single Completion		County IEA	
Producing Thru Tubing	Reservoir Temp. °F 93	Mean Annual Temp. °F 7400	Base Press. - P _a 13.2
State N.M.		Meter Run X	
L 7400	H 7400	G _g 0.647	% CO ₂ 0.98
% N ₂ 1.54	% H ₂ S 0.00	Prover	Taps

FLOW DATA						TUBING DATA		CASING DATA		Direction of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
SI							2338	70		
1.	3.00		1.50	305	8.00"	64	2226	70		1.00 Hr.
2.	3.00		1.50	305	17.00"	64	2150	70		1.00 Hr.
3.	3.00		1.50	320	32.00"	51	2088	70		1.00 Hr.
4.	3.00		1.50	330	62.00"	41	1946	70		1.00 Hr.
5.	3.00		1.50	510	90.00"	39	1650	70		1.00 Hr.

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft	Gravity Factor Fg	Super Compress. Factor Fpv	Rate of Flow Q, Mgd
1.	11.13	50.454	318.20	0.9962	1.2430	1.1000	765
2.	11.13	73.549	318.20	0.9962	1.2430	1.1000	1115
3.	11.13	103.259	333.20	1.0088	1.2430	1.1170	1610
4.	11.13	145.871	343.20	1.0188	1.2430	1.1250	2313
5.	11.13	216.998	523.20	1.0208	1.2430	1.0620	3255

NO.	P _t	Temp. °R	T _t	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.	0.47	524	1.41	0.82	41935	54.50	0.647	0.717	673	371
2.	0.47	524	1.41	0.82						
3.	0.50	511	1.38	0.79						
4.	0.51	501	1.35	0.79						
5.	0.78	499	1.35	0.886						

NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²
1.	2214.4	4904	625	
2.	2165.3	4689	840	
3.	2105.0	4431	1097	
4.	1967.5	3871	1657	
5.	1682.7	2831	2697	

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.04999$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.9122$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 6224$

Absolute Open Flow	6224	Weld @ 15.025	Angle of Slope O	47.92	Slope O	203
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Approved By Commission	Conducted By Sam Davis	Calculated By David Hany	Checked By
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RECEIVED

MAY 10 1977

U.S. DEPT. OF JUSTICE COMM.
WASH., D. C.