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appropriate district office
See Rule 401 & Rule 1122

State of New Mexico
Energy, Minerals and Natural Resources Department

Form C-122
Revised 4-1-91

OIL CONSERVATION DIVISION

P.O. Box 2088
Santa Fe, New Mexico 87504-2088

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator Meridian Oil, Inc.						Lease or Unit Name Moberly Rhodes Waterflood					
Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 11-15-95		Well No. 12			
Completion Date 11/4/95		Total Depth 3297'		Plug Back TD 3137'		Elevation		Unit Ltr. - Sec. - TWP - Rge. 20 -26- 37			
Csg. Size 7"	Wt. 20#	d	Set At 3150'	Perforations: From: 2966 To: 3103		County Lea		Pool Rhodes Yates Seven Rivers			
Tbg. Size 2-3/8"	Wt. 4.7	d	Set At 2960	Perforations: From: To:		Formation Yates Upper Gas		Connection Vented			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single						Packer Set At None		Meter Run 3.068			
Producing Thru Tbg		Reservoir Temp. °F 98°@2960		Mean Annual Temp. °F 60		Baro. Press - P _a 13.2		Taps Flg.			
L 2960	H 2960	Gg .698	% CO ₂ 3.22	% N ₂ 1.48	% H ₂ S Trace	Prover					

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
1.	3	X	1.000	50	7.00	60	262		262		24 Hours
2.	3	X	1.000	50	15.00	60	212		212		1 Hour
3.	3	X	1.000	50	19.00	60	163		164		1 Hour
4.	3	X	1.000	49	14.00	60	100		104		1 Hour
5.						60	60		64		1 Hour

RATE OF FLOW CALCULATIONS							
NO.	COEFFICIENT (24 HOUR)	$h_w P_m$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg.	Super Compress. Factor. F _{pv}	Rate of Flow Q, Mcfd
1.	4.789	21.03	63.2	1.000	1.197	1.009	122
2.	4.789	30.79	63.2	1.000	1.197	1.009	178
3.	4.789	34.65	63.2	1.000	1.197	1.009	200
4.	4.789	29.51	62.2	1.000	1.197	1.009	171
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.	.09	520	1.36	.983	DRY GAS	DRY	.698	XXXXXX	*680	*380
2.	.09	520	1.36	.983						
3.	.09	520	1.36	.983						
4.	.09	520	1.36	.983						
5.										

P _c 275.2		P _c 75.7		$1) \frac{P_c^2}{P_c^2 - P_w^2} = 1.221$ $2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.113$	
NO.	P _i ²	P _w	P _w ²	P _c ² - P _w ²	$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = .223$
1.		225.2	50.7	25.0	
2.		177.2	31.4	44.3	
3.		117.2	13.7	62.0	
4.		77.2	5.96	69.7	
5.					

Absolute Open Flow 223		Mcfd @ 15.025		Angle of Slope θ 62		Slope, n .534	
Remarks: NO FLUID PRODUCED DURING TEST							
*CORRECTED TO 3.22% CO2 and 1.48% N2							

Approved By Division	Conducted By: WEST-TEST, INC.	Calculated By: B.M.	Checked By: B.M.
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