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appropriate district office
See Rule 401 & Rule 1122

State of New Mexico
Energy, Minerals and Natural Resources Department

Form C-122
Revised 4-1-91

OIL CONSERVATION DIVISION

P.O. Box 2088
Santa Fe, New Mexico 87504-2088

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator Meridian Oil Inc.						Lease or Unit Name Moberly					
Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 8-15-95		Well No. 6			
Completion Date 8-15-95		Total Depth 3068		Plug Back TD 3060		Elevation		Unit Ltr. - Sec. - TWP - Rge. K 21-26-37			
Csg. Size 7"	Wt. d	d	Set At	Perforations: From: 2925 To: 3042				County Lea			
Tbg. Size 2-3/8	Wt. 4-7#	d 1.995	Set At 2900	Perforations: From: To:				Pool Rhodes Jalmat			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single						Packer Set At None		Formation Upper Yates			
Producing Thru TBG		Reservoir Temp. °F 91°@2900		Mean Annual Temp. °F 60°		Baro. Press - P _a 13.2		Connection Sid Richardson			
L 2900	H 2900	Gg .680	% CO ₂ 3.33	% N ₂ 1.92	% H ₂ S	Prover	Meter Run 4.026	Taps FLG			

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							350		340		24 Hours
1.	4	X	1.000	21	8.80	90	325		320		30 Min.
2.	4	X	1.000	21	13.50	96	339		331		" "
3.	4	X	1.000	21	32.00	94	331		328		" "
4.	4	X	1.000	21	50.00	90	310		309		" "
5.											

RATE OF FLOW CALCULATIONS							
NO.	COEFFICIENT (24 HOUR)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg.	Super Compress. Factor, F _{pv} .	Rate of Flow Q, Mcfd
1.	4.753	17.35	34.2	.9723	1.213	1.003	98
2.	4.753	21.49	34.2	.9671	1.213	1.003	120
3.	4.753	33.08	34.2	.9688	1.213	1.003	185
4.	4.753	41.35	34.2	.9723	1.213	1.003	232
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P. L Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure °F	Critical Temperature °F
1.	.05	550	1.47	.994	Dry	Dry	.680	XXXXXX	*678	*374
2.	.05	556	1.48	.994					P.S.I.A.	P.S.I.A.
3.	.05	554	1.48	.994						
4.	.05	550	1.47	.994						
5.										

P_c **363.2** P_c² **131.9**

NO.	P _i ²	P _w	P _w ²	P _c ² - P _w ²
1.		333.2	111.0	20.9
2.		344.2	118.5	13.4
3.		341.2	116.4	15.5
4.		322.2	103.8	28.1
5.				

1) $\frac{P_c^2}{P_c^2 - P_w^2} = 4.694$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^a = .907$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^a = 3.911$

Absolute Open Flow	.907	Mcfd @ 15.025	Angle of Slope θ	48.6	Slope, n	.8819
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Remarks: ***CORRECTED TO 3.33% CO2 & 1.92% N2**

NO FLUID PRODUCED DURING TEST

Approved By Division	Conducted By: West-Test, Inc.	Calculated By: B.M.	Checked By: B.M.
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