

## NEW MEXICO OIL CONSERVATION COMMISSION

Form C-122

## MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Revised 12-1-55

Pool Jalisco Formation Yates T-Rivers County LeonInitial \_\_\_\_\_ Annual \_\_\_\_\_ Special X Date of Test 4-25-1958Company El Paso Natural Gas Company Lease Huberly "C" Well No. 3Unit 8 Sec. 21 Twp. 26 Rge. 37 Purchaser El Paso Natural Gas CompanyCasing 5 1/2" Wt. 17.0 I.D. \_\_\_\_\_ Set at 3097 Perf. \_\_\_\_\_ To \_\_\_\_\_Tubing 2" Wt. 6.7 I.D. \_\_\_\_\_ Set at 3130 Perf. \_\_\_\_\_ To \_\_\_\_\_Gas Pay: From 3124 To 3126 L 3097 xG .695 -GL 2152 Bar.Press. 13.2Producing Thru: Casing X Tubing \_\_\_\_\_ Type Well Single

Single-Bradenhead-G. G. or G.O. Dual

Date of Completion: 4-22-1958 Packer None Reservoir Temp. \_\_\_\_\_

## OBSERVED DATA

Tested Through (Pressure) (Choke) (Meter) Type Taps 7/8"

Flow Data						Tubing Data		Casing Data		Duration of Flow Hr.
No.	(Prover) (Line) Size	(Choke) (Orifice) Size	Press. psig	Diff. h <sub>w</sub>	Temp. °F.	Press. psig	Temp. °F.	Press. psig	Temp. °F.	
SI										
1.	1"	1.500	510	2.25	72	505		571		24
2.	1"	1.500	505	1.00	65	498		506		24
3.	1"	1.500	514	1.20	64	502		522		24
4.	1"	1.500	514	7.29	69	507		537		24
5.										

## FLOW CALCULATIONS

No.	Coefficient (24-Hour)	$\sqrt{h_w p_f}$	Pressure psia	Flow Temp. Factor F <sub>t</sub>	Gravity Factor F <sub>g</sub>	Compress. Factor F <sub>pv</sub>	Rate of Flow Q-MCFPD @ 15.025 psia
1.	11.99	24.95	513.2	.9897	.9992	1.001	176
2.	11.99	15.92	514.2	.9992	.9992	1.001	63
3.	11.99	17.24	513.2	.9993	.9992	1.002	68
4.	11.99	61.94	517.2	.9995	.9992	1.002	249
5.							

## PRESSURE CALCULATIONS

Gas Liquid Hydrocarbon Ratio \_\_\_\_\_ cf/bbl.

Gravity of Liquid Hydrocarbons \_\_\_\_\_ deg.

F<sub>c</sub> 1.812 (1-e<sup>-s</sup>) .138

Specific Gravity Separator Gas \_\_\_\_\_

Specific Gravity Flowing Fluid \_\_\_\_\_

P<sub>c</sub> 680.2 P<sub>c</sub><sup>2</sup> 356.4

No.	P <sub>w</sub> psia	P <sub>t</sub> <sup>2</sup>	F <sub>c</sub> Q	(F <sub>c</sub> Q) <sup>2</sup>	(F <sub>c</sub> Q) <sup>2</sup> (1-e <sup>-s</sup> )	P <sub>w</sub> <sup>2</sup>	P <sub>c</sub> <sup>2</sup> -P <sub>w</sub> <sup>2</sup>	Cal. P <sub>w</sub>	P <sub>w</sub> / P <sub>c</sub>
1.	513.2	263.3	.853	.728	.709	263.3	13.2	513.3	98.1
2.	514.2	264.4	1.189	1.414	.134	264.4	114.8	519.1	99.1
3.	513.2	263.3	1.174	1.378	.140	263.3	98.9	515.4	98.9
4.	517.2	267.7	1.538	2.365	.346	267.7	81.6	519.5	98.5
5.									

Absolute Potential: 2.850 MCFPD; n .771COMPANY El Paso Natural Gas CompanyADDRESS P. O. Box 1384, Del. New MexicoAGENT and TITLE R. T. Wright - Petroleum EngineerWITNESSED J. B. Murray & J. O. WhittingCOMPANY El Paso Natural Gas Company

## REMARKS

\* No Point alignment. Average Jalisco slope of .771 drawn through the highest rate of flow.

This is a corrected copy of test previously sent out.

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

- $Q$  = Actual rate of flow at end of flow period at W. H. working pressure ( $P_w$ ).  
MCF/da. @ 15.025 psia and 60° F.
- $P_c$  = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater.  
psia
- $P_w$  = Static wellhead working pressure as determined at the end of flow period.  
(Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- $P_t$  = Flowing wellhead pressure (tubing if flowing through tubing, casing if  
flowing through casing.) psia
- $P_f$  = Meter pressure, psia.
- $h_w$  = Differential meter pressure, inches water.
- $F_g$  = Gravity correction factor.
- $F_t$  = Flowing temperature correction factor.
- $F_{pv}$  = Supercompressability factor.
- $n$  = Slope of back pressure curve.

Note: If  $P_w$  cannot be taken because of manner of completion or condition of well, then  $P_w$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_t$ .