

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special		Date 8-29-75	
Company Doyle Hartman		Connection None	
Pool Jalmat		Formation Yates	
Completion Date 4 3 75		Total Depth 3650	Plug Back TD 3010
Elevation 2913 g1		Farm or Lease Name Spear St.	
Csq. Size 4 1/2	Wt. 10.5	d 	Set At 3650
Perforations: From 2661 To 2931		Well No. #1	
Tbg. Size 2 3/8	Wt. 4.7	d 	Set At 2930
Perforations: From Open To end		Unit Sec. Twp. Rge. F 2 26 37	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single		Packer Set At None	
County Lea		State N.M.	
Producing Thru TBG *	Reservoir Temp. °F 85 @ 2700	Mean Annual Temp. °F 	Baro. Press. - P _a
L 2796	H 2796	Gg .650	% CO ₂ % N ₂ % H ₂ S Prover 2"
Meter Run		Type	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							545		545		72 Hr.
1.	2 x 1/16			480		82	480		480		1 Hr.
2.	2 x 3/32			344		78	400		344		1 Hr.
3.	2 x 1/8			220		84	340		220		1 Hr.
4.	2 x 3/16			170		87	320		170		1 Hr.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	.06405		493.2	.9795	1.240	1.044	40
2	.1410		357.2	.9831	1.240	1.033	63
3	.2648		233.2	.9777	1.240	1.021	76
4	.6082		183.2	.9750	1.240	1.015	137
5							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Dry _____ Mcf/bbl.
1	.74	542	1.45	.917	A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2	.53	538	1.43	.937	Specific Gravity Separator Gas _____ .650 X X X X X X X X
3	.35	544	1.45	.959	Specific Gravity Flowing Fluid _____ X X X X X
4	.27	547	1.46	.970	Critical Pressure _____ 670 _____ P.S.I.A. _____ P.S.I.A.
5					Critical Temperature _____ 375 _____ R _____ R

NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.212$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.101$
1		493.2	243.2	68.4	AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = .084$	
2		357.2	127.6	184.0		
3		233.2	54.4	257.2		
4		183.3	33.6	278.0		
5						

Absolute Open Flow	84	Mcf/d @ 15.025	Angle of Slope	63.5	Slope, n	.500
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Remarks: No fluid made during test.
* Well tested through casing. P_w calculated from flowing casing pressure due to fluid in the tubing.

Approved By Commission: <i>John W. Runyan</i>	Conducted By: Rick Pagan	Calculated By: Rick Pagan	Checked By:
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