

ORIGINAL

NEW XICO OIL CONSERVATION COMMISSION MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-124
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 2-24-73			
Company Texas West Oil & Gas Co.				Connection None					
Pool Wildcat				Formation Atoka				Unit	
Completion Date 3/6/73		Total Depth 12,473'		Plug Back TD 12,350'		Elevation 3465.5 GR		Farm or Lease Name State "2" Com.	
Csg. Size 5-1/2"	Wt. 19.81#	d 4.778"	Set At 12,464'	Perforations: From 12,288' To 12,302'		Well No. 1			
Tbg. Size 2-7/8"	Wt. 6.5#	d 2.441"	Set At 12,240'	Perforations: From To		Unit Sec. Twp. Rge. E 2 24-S 34-E			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single						Packer Set At 12,240'		County Lea	
Producing Thru 2-7/8" Tbg		Reservoir Temp. °F 205 ^o 12,300'		Mean Annual Temp. °F		Baro. Press. - P _a 15.2		State New Mexico	
L 11,800	H 11,800	Gg .721	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run X	Taps	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							7013.2	60			
1.	4		2.5	900	23	45	6158	60			3.417 Hrs
2.				900	16	82	6117	60			2.25 Hrs
3.				920	30	72	5450	60			2.0 Hrs
4.				920	42	65	5050	60			2.0 Hrs
5.				925	46	67	4650	60			3.5 Hrs

RATE OF FLOW CALCULATIONS Gas Produced 3948 Mcf							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	32.64	143.87	913.2	1.015	1.178	1.098	6165
2	32.64	120.87	913.2	.9795	1.178	1.106	5035
3	32.64	166.13	933.2	.9887	1.178	1.116	7048
4	32.64	196.57	933.2	.9952	1.178	1.125	8462
5	32.64	206.29	938.2	.9933	1.178	1.125	8863

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio 16395 Mcf/bbl.			
1	1.37	505	1.28	.829	A.P.I. Gravity of Liquid Hydrocarbons 57.2 Deg.			
2	1.37	542	1.37	.817	Specific Gravity Separator Gas X X X X X X X X			
3	1.40	532	1.35	.803	Specific Gravity Flowing Fluid X X X X X			
4	1.40	525	1.33	.790	Critical Pressure 668 P.S.I.A. P.S.I.A.			
5	1.40	527	1.33	.790	Critical Temperature 395 R R			

NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \frac{49352}{10607}$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{4.270}{}$
1		6048.5	36584	12768	AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{21499}{}$	
2		6224.6	38745	10607		
3		5783.0	33443	15909		
4		5455.2	29759	19593		
5		5171.7	26746	22606		

Absolute Open Flow 21499 Mcfd @ 15.025		Angle of Slope @ 46° 39'		Slope, n .944	
Remarks:					
Approved By Commission: Conducted By: D. F. Jones Calculated By: H. L. Hagler Checked By:					