

**N MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL**

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 2/23/89			
Company Enron Oil & Gas Company				Connection Transwestern Pipeline Co.					
Pool West Pitchfork Ranch				Formation Atoka				Unit	
Completion Date 2/18/89		Total Depth 14,698		Plug Back TD 13,725		Elevation 3573' GR		Farm or Lease Name Government L Com.	
Csg. Size 5-1/2"	Wt. 23#	Set At 4.670	Set At 14108	Perforations: From 13496 To 13530				Well No. 2	
Tub. Size 2-7/8	Wt. 6.5#	Set At 2.441	Set At 13260	Perforations: From Open ended To				Unit Sec. Twp. Rge. K 18 24S 34E	
Type Well - Single - Bradenhead - G.C. or G.O. Multiple Single						Packer Set At 13260		County Lea	
Producing Thru Tubing		Reservoir Temp. °F 189 @ 13496		Mean Annual Temp. °F 60.0		Baro. Press. - P _a 13.2		State New Mexico	
L 13496	H 13496	G _g .616	% CO ₂ .20	% N ₂ .87	% H ₂ S .00	Prover .0	Meter Run 4.026	Taps Flange	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							7622	60	Packer		100.0
1.	4.00 x 1.750			895	9.0	64	6375	64	"	0	1.0
2.	4.00 x 1.750			895	21.0	66	5685	66	"	0	1.0
3.	4.00 x 1.750			900	33.0	70	5030	70	"	0	1.0
4.	4.00 x 1.750			905	49.0	72	4350	72	"	0	1.0
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	14.94	90.41	908.2	.9962	1.2741	1.0825	1855
2	14.94	138.10	908.2	.9943	1.2741	1.0811	2825
3	14.94	173.60	913.2	.9905	1.2741	1.0790	3531
4	14.94	212.11	918.2	.9887	1.2741	1.0782	4303
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio 294 Mcf/bbl.	A.P.I. Gravity of Liquid Hydrocarbons 56 @ 60°F Deg.	Specific Gravity Separator Gas .616	Specific Gravity Flowing Fluid .625	Critical Pressure 671 P.S.I.A.	Critical Temperature 361 R
1	1.35	524	1.45	.853						
2	1.35	526	1.46	.856						
3	1.36	530	1.47	.859						
4	1.37	532	1.47	.860						
5.										

NO.	P _r ²	P _w	P _w ²	P _r ² - P _w ²
1		6394	40877	17419
2		5708	32576	25721
3		5054	25542	32755
4		4381	19195	39101
5				

(1) $\frac{P_r^2}{P_r^2 - P_w^2} = 1.4909$

(2) $\left[\frac{P_r^2}{P_r^2 - P_w^2} \right]^n = 1.4909$

AOF = $\left[\frac{P_r^2}{P_r^2 - P_w^2} \right]^n = 6415$

P_c 7635.2 P_c² 58296

Absolute Oper. Flow 6415 Mcfd @ 15.025	Angle of Slope 45.0	Slope, n 1.000
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Remarks: **MAR 3 1989**

Approved By: **JERRY SEXTON** Conducted By: **Jarrel Services, Inc.** Calculated By: **Computer** Checked By: **LWH Barry Seldon**

DISTRICT I SUPERVISOR

3/1/89 Enron oil & Gas Co.