

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form O-1
Revised 9-1-74

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 6-17-82	
Company The Superior Oil Company				Connection PipeLine			
Pool South Bell Lake				Formation Morrow			
Completion Date 6-2-82		Total Depth 15,007		Plug Back TD 14,916		Elevation	
Casing Size 4 1/2" Liner		Wt. 13.5		Set At 14612		Perforations: From 14,546 To 14592	
Tub. Size 2 7/8"		Wt. 6.5		Set At 14250		Perforations: From OPENENDED	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE						Packer Set At 14,250	
Producing Thru Tubing		Reservoir Temp. °F 60°		Mean Annual Temp. °F 60°		Baro. Press. - P _a 13.2	
L 14,569		H 14,569		G _g .5931		% CO ₂ .741	
				% N ₂ .299		% H ₂ S	
				Prover		Meter Run 2.067	
						Taps Flange	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							3229		PKR	CHOKE	24 Hou
1.	2.067	x	1.125	755	5"	59°	2643			5/64	1 Hr.
2.	2.067	x	1.125	755	10	56	2310			7/64	1 Hr.
3.	2.067	x	1.125	755	17	54	1955			9/64	1 Hr.
4.	2.067	x	1.125	755	28	54	1535			11/64	1 Hr.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	6.393	61.98	768.2	1.001	1.299	1.065	549
2	6.393	87.65	768.2	1.004	1.299	1.067	780
3	6.393	114.28	768.2	1.006	1.299	1.069	1021
4	6.393	146.66	768.2	1.006	1.299	1.069	1310
5							

NO.	R	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/b		
					A.P.L. Gravity of Liquid Hydrocarbons _____ D		
					Specific Gravity Separator Gas _____ 5931 XXXXXXXX		
					Specific Gravity Flowing Fluid _____ XXXXX		
					Critical Pressure _____ 676 P.S.I.A. P.S.I.		
NO.	R	Temp. °R	T _r	Z	Critical Temperature _____ 354 R		

$(1) \frac{P_c^2}{P_c^2 - P_w^2} = \frac{1.3151}{1.3151 - 1.273} = 1.3151$				$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{1.3151}{1.3151 - 1.273} = 1.3151$			
$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1,723$							

NO.	P _i ²	P _w ²	P _c ²	P _c ² - P _w ²
1		2709	7339	3173
2		2358	5560	4952
3		2051	4207	6305
4		1587	2519	7993
5				

Absolute Open Flow _____ 1,723 _____ Mcfd @ 15.025		Angle of Slope θ _____ 45°		Slope, n _____ 1.00	
Remarks: _____					
Approved By Commission:		Conducted By: J.W.		Calculated By: M.K.	
				Checked By: M.K.	

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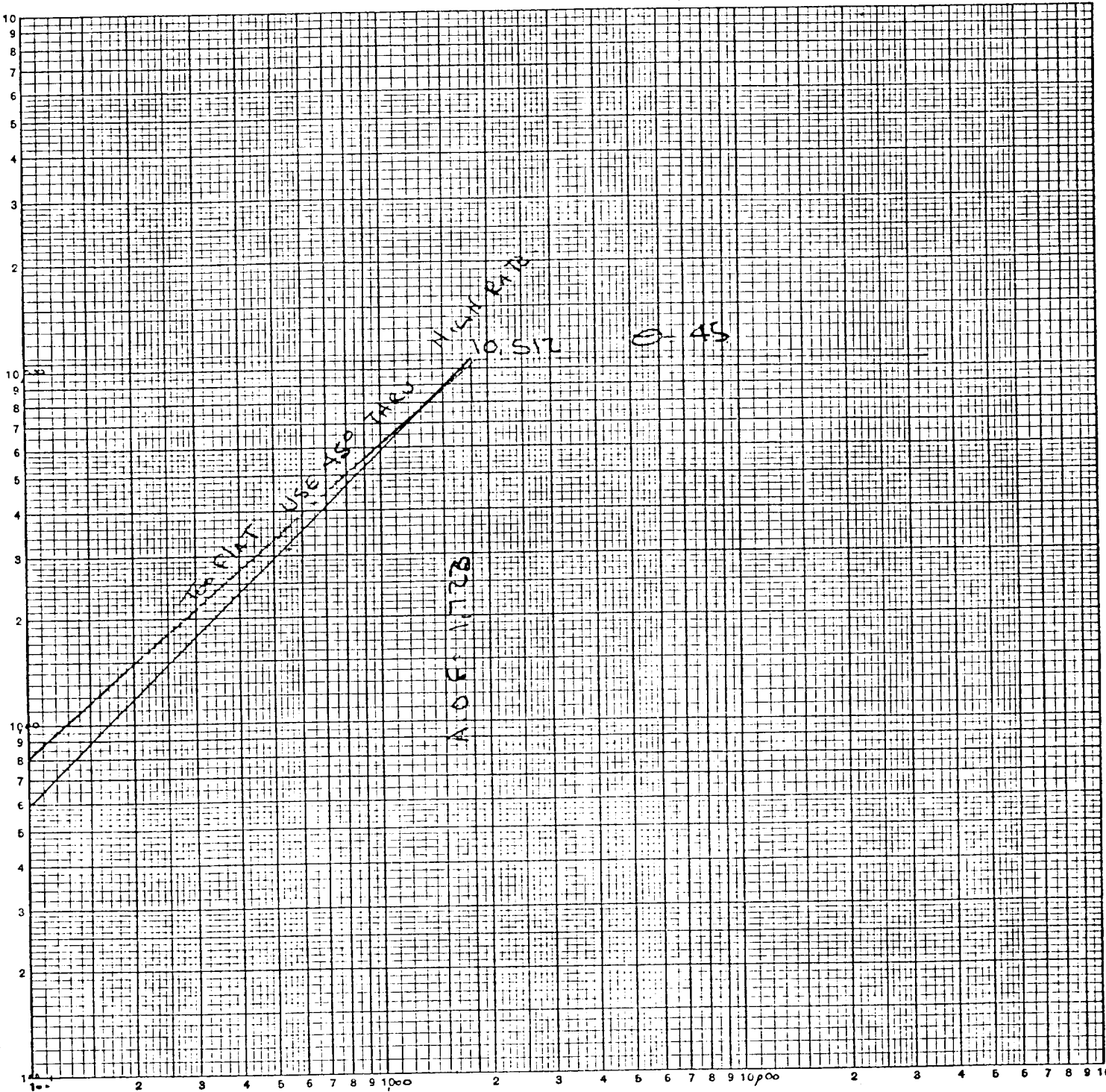
AUG 31 1982

G.C.D.
HOBBY OFFICE

$$1310 \left(\frac{10,512}{7993} \right)^{1.000} = 1723.$$

P₂-82

LOGARITHMIC
40 / 400
3 X 3 CYCLES
KEUFFEL & ESSER CO.



UC.F107.

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