

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 6-17-86	
Company Southland Royalty Company		Connection To Air	
Pool Johnson Ranch		Formation Wolfcamp	
Completion Date 6-7-86		Total Depth 15694	Plug Back TD 14,765
Elevation 3522.4' GR		Farm or Lease Name Madera Ridge "27" St Com	
Ceq. Size 7 & 4 1/2	Wt. 15.1	Set At 14,765	Perforations: From 13,266 To 13,532
Tbg. Size 2 7/8	Wt. 6.5	Set At 12,798	Perforations: From Open To End
Type Well - Single - Brdenhead - G.G. or G.O. Multiple Single		Packer Set At 12,687	Unit B
Producing Thru Tbg	Reservoir Temp. °F 207.0 @ 13,266	Mean Annual Temp. °F 60	Baro. Press. - P _a 13.2
L 12,798	H 12,798	G _g .639	% CO ₂ .295
		% N ₂ .650	% H ₂ S -
		Prover -	Meter Run 4"
			Taps Flg.

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							7984	(SIP)			
1.	4 x 1.250			440	15	82	7690				72 HRS.
2.	4 x 1.250			440	28	60	7070				1 HR
3.	4 x 1.250			440	60	60	6300				1 HR
4.	4 x 1.250			600	79	60	5302				1 HR
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow O, Mcfd
1	7.469	82.45	453.2	.9795	1.251	1.041	785
2	7.469	112.65	453.2	1.00	1.251	1.047	1102
3	7.469	164.90	453.2	1.00	1.251	1.047	1613
4	7.469	220.10	613.2	1.00	1.251	1.063	2186
5							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1	.68	540	1.45	.923	25.752	52 @ 60	.639	X X X X X X X X	670	372
2	.68	520	1.40	.913				X X X X X		
3	.68	520	1.40	.913						
4	.92	520	1.40	.885						
5										

NO.	P _i ²	P _w	P _w ²	P _i ² - P _w ²
1	7703.2	59339.2	4616.0	
2	7083.2	50171.7	13783.5	
3	6313.2	39856.5	24098.7	
4	5315.2	28251.4	35703.8	
5				

(1) $\frac{P_c^2}{P_i^2 - P_w^2} = 1.791$

AOF = Q $\left[\frac{P_c^2}{P_i^2 - P_w^2} \right]^n = 3.265$

(2) $\left[\frac{P_c^2}{P_i^2 - P_w^2} \right]^n = 1.493$

Absolute Open Flow	3,265	Mcfd @ 15.025	Angle of Slope @	55 1/2	Slope, n	.688
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Remarks: 9.2 Bbls of condensate during test. Calculations for P_w were attempted but were lower than flowing tbg press. Flwg tbg press were used for P_w. Due to large amount of fluid.

Approved By Division	Conducted By:	Calculated by:	Checked By:
ORIGINAL SIGNED BY JERRY SEXTON	Reston, Jackson & Golden	R. E. Reston	
DISTRICT SUPERVISOR			