

OIL CONSERVATION DIVISION

STATE OF NEW MEXICO
ENERGY AND MINERALS DEPARTMENTP. O. BOX 2088
SANTA FE, NEW MEXICO 87501Form C-122
Revised 10-1-78

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 5-19-90	
Company TEXACO PRODUCING INC.			Connection SALES		
Pool JALMAT T-Y-SR			Formation JALMAT, UPPER		Unit
Completion Date 5-15-90		Total Depth 3245'	Plug Back TD 3240'	Elevation GR-3390	Farm or Lease Name EUGENE COATS
Ceq. Size 5.5"	Wt. 15.5#	d 4.950	Set At 3245	Perforations: From 2950' To 3200'	Well No. 8
Thg. Size 2.375	Wt. 4.7#	d 1.995	Set At 2889	Perforations: From To	Unit Sec. Twp. Rge. J 3 24-S 36-E
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE G.G.				Packer Set At 2889'	County LEA
Producing Thru TUBING		Reservoir Temp. °F 100 @ 3240	Mean Annual Temp. °F 60	Baro. Press. - P _a 13.2	State NEW MEXICO
L 2889	H 2889	G _g .760	% CO ₂ 0.13	% N ₂ 23.53	% H ₂ S Prover Meter Run Taps 3.068 FLANGE

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI	3.068		1.750				615	80	PACKER		SI 48 m
1.	3.068		1.750	90	10	68	575	70			1.0 m
2.	3.068		1.750	110	18	68	550	70			1.0 m.
3.	3.068		1.750	100	37	67	509	68			1.0 m.
4.	3.068		1.750	90	72	67	432	68			1.0 m.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	15.61	32.12	103.2	.9924	1.147	1.010	576
2	15.61	47.09	123.2	.9924	1.147	1.010	845
3	15.61	64.72	113.2	.9933	1.147	1.010	1162
4	15.61	86.20	103.2	.9933	1.147	1.010	1548
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1	.20	528	1.53	.981	A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2	.20	528	1.53	.981	Specific Gravity Separator Gas .760 XXXXXXXXXX
3	.20	527	1.53	.981	Specific Gravity Flowing Fluid XXXXX
4	.20	527	1.53	.981	Critical Pressure 626 P.S.I.A. P.S.I.A.
5.					Critical Temperature 345 R R

P_c 628.2 P_c^2 394.6 NO. P_i^2 P_w P_w^2 $P_c^2 - P_w^2$					$(1) \frac{P_c^2}{P_c^2 - P_w^2} = \frac{394.6}{105.9}$		$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3.1125$	
1	346.0	591.5	349.9	44.7	$AOI = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3616$			
2	317.2	570.7	325.7	68.9				
3	272.7	537.3	288.7	105.9				
4	198.2	476.1	226.7	167.9				
5								

Absolute Open Flow	3616	Mcfd @ 15.025	Angle of Slope	49.2°	Slope, n	.8632
Remarks:						

Approved By Division	Conducted By J.E. Bryant/rmn	Calculated By TM/Morgan	Checked By:
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