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See Rule 401 & Rule 1122

State of New Mexico
Energy, Minerals and Natural Resources Department

Form C-122
Revised 4-1-91

OIL CONSERVATION DIVISION

P.O. Box 2088
Santa Fe, New Mexico 87504-2088

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator GRUY Petroleum					Lease or Unit Name Rhodes 23 Federal Com.				
Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 9-5-97		Well No. 1		
Completion Date 9-4-97		Total Depth 3265		Plug Back TD 3242		Elevation 2984		Unit Ltr. - Sec. - TWP - Rgc. M 23-26S-37E	
Csg. Size 4 1/2	Wt. 11.6	d 4.000	Set At 3265	Perforations: From: 2894 To: 3104				County Lea	
Tbg. Size 2-3/8	Wt. 4.7	d 1.995	Set At 2893	Perforations: Open Ended				Pool Rhodes Gas	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single					Packer Set At None		Formation Yates-Seven Rivers		
Producing Thru Tubing		Reservoir Temp. °F 82		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2		Connection To Air	
L 2893	H 2893	G _g 0.678	% CO ₂ 2.22	% N ₂ 1.49	% H ₂ S	Pressure Positive Choke 6" Nipple		Rock	

FLOW DATA					TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI						219	63	220	63	70 Hrs
1.	8/64	0.2618				207	62	204	62	1 Hr.
2.	12/64	0.6101				190	62	193	62	1 Hr.
3.	16/64	1.112				180	61	181	61	1 Hr.
4.	20/64	1.771				158	63	169	63	1 Hr.
5.										

RATE OF FLOW CALCULATIONS							
NO.	COEFFICIENT (24 HOUR)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	0.2618		220.2	0.99811	1.214	1.022	71.39
2.	0.6101		203.2	0.99811	1.214	1.020	153.07
3.	1.112		193.2	0.9990	1.214	1.020	265.76
4.	1.771		171.2	0.9971	1.214	1.017	373.25
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Dry Gas	Mc/bbl
1.	.33	522	1.39	0.957	A.P. L Gravity of Liquid Hydrocarbons	Dry Gas	De
2.	.31	522	1.39	0.961	Specific Gravity Separator Gas	0.678	XXXXXXXXXX
3.	.29	521	1.39	0.962	Specific Gravity Flowing Fluid	XXXXXX	
4.	.25	523	1.39	0.967	Critical Pressure	*676	PSIA
5.					Critical Temperature	*376	R

P _c 233.2 P _a 54.38				
NO.	P _i ²	P _w	P _w ²	P _a ² - P _w ²
1.		217.2	47.18	7.21
2.		206.2	42.52	11.86
3.		194.2	37.71	16.67
4.		182.2	33.20	21.19
5.				

1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.566$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^* = 957.87$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^* = 2.566$

Absolute Open Flow	958	Mcfd @ 15.025	Angle of Slope θ	45°	Slope, n	1.000
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Remarks: *Corrected to 2.22% CO₂ and 1.49% N₂

Approved By Division	Conducted By:	Calculated By:	Checked By:
	MCT	TR	TR