

Oil Conservation Division
1220 South St. Francis Dr.
Santa Fe, NM 87505

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator Gruy Petroleum Mgt. Company						Lease or Unit Name : Myers "B"					
Type Test x ☐ Initial ☐ Annual ☐ Special						Test Date 4-26-01					
Completion Date 4-26-01			Total Depth 3885			Plug Back TD 3868			Elevation 3369		
Csg. Size 5 1/2			Wt. 15.5			Set At 3868			Perforations: From: 3136-56 To: 3356-3434		
Thg. Size 2 3/8			Wt. 4.7			Set At 3128			Perforations: From: open ended To:		
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE						Packer Set At None					
Producing Thru Tubing			Reservoir Temp. °F 108 @ 3434			Mean Annual Temp. °F 60			Baro. Press - P _a 13.2		
L 3128			H 3128			Gg .665			%CO ₂ 2.340		
						%N ₂ 3.909			%H ₂ S		
						Prover			Meter Run 4.026		
									Taps Flange		

FLOW DATA					TUBING DATA		CASING DATA		Duration Of Flow
No.	Prover Line Size	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
SI						442	73	442	
1.	4.026 X 1.250		8	77	98	155	75	348	
2.	4.026 X 1.250		8	60.8	98	170	75	355	60 MIN
3.	4.026 X 1.250		8	36	95	198	74	360	60 MIN
4.	4.026 X 1.250		8	17.6	95	252	72	388	60 MIN
5.									60 MIN

RATE OF FLOW CALCULATIONS							
No.	COEFFICIENT (24 HOUR)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	7.469	40.40	21.2	.9653	1.226	Nil	357
2.	7.469	35.90	21.2	.9653	1.226	Nil	317
3.	7.469	27.63	21.2	.9860	1.226	Nil	249
4.	7.469	19.3	21.2	.9860	1.226	Nil	174
5.							

No.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1.	.03	558	1.48	Nil	A. P. I. Gravity of Liquid Hydrocarbons	
2.	.03	558	1.48	Nil	Specific Gravity Separator Gas .665	
3.	.03	555	1.47	Nil	Specific Gravity Flowing Fluid XXXXX	XXXXXXXXXX
4.	.03	555	1.47	Nil	Critical Pressure .670	P.S.I.A.
5.					Critical Temperature .378	P.S.I.A.

No.	P _c 455	P _c ² 207	P _w ²	P _c ² - P _w ²
1.	28.3	361.2	130.3	76.9
2.	33.6	368.2	135.6	71.6
3.	44.5	373.2	139.3	67.9
4.	70.2	401.2	161.0	46.2
5.				

(1) P₂ = 2.694

$\frac{P_c^2 - P_w^2}{P_c^2 - P_w^2}$

AOF = Q

$\left[\frac{P_c^2}{P_c^2 - P_w^2} \right] = 961$

(2) P_c² = 2.694

$\frac{P_c^2 - P_w^2}{P_c^2 - P_w^2}$

Absolute Open Flow 961		Mcf/d @ 15.025		Angle of Slope θ: 45		Slope, n: 1.00	
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Remarks: High Rate was conducted first due to high fluid entry. Fluid made during each rate 3 bbls per hour.

Approved By Division	Conducted By: Reggie Reston	Calculated By: Reggie Reston	Checked By:
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BUREAU OF LAND MGMT
ROSWELL OFFICE

JUL 20 AM 10:05

RECEIVED



JUL 20
RECEIVED
Hobbs
OCD