

## NEW MEXICO OIL CONSERVATION COMMISSION

HOBBS OFFICE OCC

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Form C-122

MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Revised 12-1-55

Pool Jalnet Formation Tanabe County LeaInitial Annual Special X Date of Test 4,8-12,57Company Southern California Petr. Lease Gutman Well No. 1Unit 0 Sec. 18 Twp. 24 Rge. 37 Purchaser El Paso Natural Gas CompanyCasing 5 1/2" Wt. 14 I.D. 5.012 Set at 3350' PB Perf. 2948' To 3048'Tubing 2 3/8" Wt. 4.7 I.D. 1.995 Set at 2978' Perf. - To -Gas Pay: From 2948' To 3048' L 2948' xG .640 -GL 1906 Bar.Press. 13.2Producing Thru: Casing Re Tubing X Type Well SingleDate of Completion: 2-17-57 Packer 2918' Single-Bradenhead-G. G. or G.O. Dual  
Reservoir Temp. -

## OBSERVED DATA

Tested Through (Prover) (Choke) (Meter) Type Taps Flange

No.	Flow Data					Tubing Data		Casing Data		Duration of Flow Hr.
	(Line) Size	(Orifice) Size	Press. psig	Diff. h <sub>w</sub>	Temp. °F.	Press. psig	Temp. °F.	Press. psig	Temp. °F.	
SI						<u>745</u>				<u>72</u>
1.	<u>4</u>	<u>.750</u>	<u>522</u>	<u>22.1</u>	<u>61</u>	<u>610</u>				<u>24</u>
2.	<u>4</u>	<u>.750</u>	<u>528</u>	<u>25.0</u>	<u>63</u>	<u>597</u>				<u>24</u>
3.	<u>4</u>	<u>.750</u>	<u>524</u>	<u>30.3</u>	<u>71</u>	<u>574</u>				<u>24</u>
4.	<u>4</u>	<u>.750</u>	<u>512</u>	<u>41.0</u>	<u>58</u>	<u>520</u>				<u>24</u>
5.										

## FLOW CALCULATIONS

No.	Coefficient (24-Hour)	$\sqrt{h_w P_f}$	Pressure psia	Flow Temp. Factor F <sub>t</sub>	Gravity Factor F <sub>g</sub>	Compress. Factor F <sub>pv</sub>	Rate of Flow Q-MCFPD @ 15.025 psia
1.	<u>3.435</u>	<u>108.71</u>	<u>535.2</u>	<u>.9990</u>	<u>.9682</u>	<u>1.055</u>	<u>381</u>
2.	<u>3.435</u>	<u>116.30</u>	<u>541.2</u>	<u>.9971</u>	<u>.9682</u>	<u>1.055</u>	<u>407</u>
3.	<u>3.435</u>	<u>127.45</u>	<u>537.2</u>	<u>.9896</u>	<u>.9682</u>	<u>1.051</u>	<u>441</u>
4.	<u>3.435</u>	<u>146.64</u>	<u>525.2</u>	<u>1.0019</u>	<u>.9682</u>	<u>1.053</u>	<u>514</u>
5.							

## PRESSURE CALCULATIONS

Gas Liquid Hydrocarbon Ratio - cf/bbl.  
Gravity of Liquid Hydrocarbons - deg.  
F<sub>c</sub> 9.936 (1-e<sup>-s</sup>) 0.123Specific Gravity Separator Gas -  
Specific Gravity Flowing Fluid -  
P<sub>c</sub> 758.2 P<sub>c</sub> 574.9

No.	P <sub>t</sub> (psia)	P <sub>t</sub> <sup>2</sup>	F <sub>c</sub> Q	(F <sub>c</sub> Q) <sup>2</sup>	(F <sub>c</sub> Q) <sup>2</sup> (1-e <sup>-s</sup> )	P <sub>w</sub> <sup>2</sup>	P <sub>c</sub> <sup>2</sup> -P <sub>w</sub> <sup>2</sup>	Cal. P <sub>w</sub>	P <sub>w</sub> /P <sub>c</sub>
1.	<u>623.2</u>	<u>388.4</u>	<u>3.786</u>	<u>14.33</u>	<u>1.76</u>	<u>390.2</u>	<u>184.7</u>		
2.	<u>610.2</u>	<u>372.3</u>	<u>4.043</u>	<u>16.35</u>	<u>2.01</u>	<u>374.3</u>	<u>200.6</u>		
3.	<u>587.2</u>	<u>344.8</u>	<u>4.382</u>	<u>19.20</u>	<u>2.36</u>	<u>347.2</u>	<u>227.7</u>		
4.	<u>533.2</u>	<u>284.3</u>	<u>5.107</u>	<u>26.08</u>	<u>3.21</u>	<u>287.5</u>	<u>287.4</u>		
5.									

Absolute Potential: 840 MCFPD; n .689COMPANY Southern California Petroleum CorporationADDRESS Box 1071, Midland, TexasAGENT and TITLE Joe A. Coleman, P.E., New Mexico, Cert. No. 2208WITNESSED -COMPANY Neal-Coleman Engineering Company

REMARKS

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

$Q$  = Actual rate of flow at end of flow period at W. H. working pressure ( $P_w$ ).  
MCF/da. @ 15.025 psia and 60° F.

$P_c$  = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater.  
psia

$P_w$  = Static wellhead working pressure as determined at the end of flow period.  
(Casing if flowing thru tubing, tubing if flowing thru casing.) psia

$P_t$  = Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia

$P_f$  = Meter pressure, psia.

$h_w$  = Differential meter pressure, inches water.

$F_g$  = Gravity correction factor.

$F_t$  = Flowing temperature correction factor.

$F_{pv}$  = Supercompressibility factor.

$n$  = Slope of back pressure curve.

Note: If  $P_w$  cannot be taken because of manner of completion or condition of well, then  $P_w$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_t$ .