MULTI-POINT BACK PRESSURE TEST FOR PAS WILLS: 39

Revised 12-1-55

	ormation <u>Paddock</u>				County Lea					
									Tune 2-6, 196	
ompany Gulf O	11 Corpora	tion	<u>-</u>	Lease Pl	laine-Kn	lght	We	ll No	3	
nit L	Sec. 23	Two. 24						_		
sing 5.5								To 4	. e	
bing 2										
s Pay: From	4839 To	4845	T. 47	793 x	G 700 (8	rasumed)	2255	Pon D.	ess. <u>13.2</u>	
oducing Thru										
Recomp. te of Complet	tion: <u>1/21/</u>	/62	Packe	r	Sin	gle_Brade Reserve	enhead-G.	G. or	G.O. Dual	
					ED DATA		-			
sted Through	(Prover)	(Cheke)	x(Motor)				Type Tap	os		
	Flow				Tubing	Data	Casing I	ata		
(Prover)	(Orifice))	Diff.	•		Temp.	Press.	Temp.	of Flo	
Size	Size	psig	h _w	°F.		°F.	psig	°F∙	Hr.	
2	,250	197		97	<u> 1643</u> 1543	 	1646	 	72	
2	.500	89	†	98	1376		1547 1388	 		
2	.500	117		94	1264		1276	 	3	
2	.500	127		97	814		887		3	
	.250	226	L1	104	1355		1415			
			I	FLOW CALC	CULATION	S				
Coeffici	ent	Pr	ressure Flow Tem		Cemp.	Gravity Compre		ss. Rate of Flow		
(24-Hour) 7		h _w p _f psia		Fact	cor	Factor	Factor		Q-MCFPD	
	$V \setminus V \cap V$	w ^p f	psia	F _t	;	$^{ extsf{F}_{ extsf{g}}}$	Fpv		@ 15.025 psi	
1,4030			10.2	.9662		.9258	1.019		269	
5.5233			02.2	.9653		9258	1,000		505	
5.5233 5.5233			30.2	9688		-9258	1.012		653	
1,4030			40.2 39.2	.9662 .9602		-9258 -9258	1.012		701	
							1.020	· · · · · · · · · · · · · · · · · · ·	32930V	
iquid Hydrod	carbon Rati	io None		CSSURE CA	LCU!ATIO	Speci	fic Gravit	ty Sepa	rator Gas	
Liquid Hydrod ity of Liquid Magured	d Hydrocarb	io <u>None</u> bons (1-e ^{-s})			LCU! ATIC	Speci Speci	fic Gravi fic Gravit	ty Sepa ty Flow PC	ing Fluid non	
P _w (psia)	d Hydrocart	oons		cf/bbldeg(Fc	Q) ² e ⁻³)	Speci Speci	fic Gravit	ry Flow PC 2	ring Fluid non	
P _w (psia)	d Hydrocart	oons(1-e ^{-s})		cf/bbldeg(Fc	Q) ² e ⁻³)	Speci Speci Pc Pw ²	fic Gravit 659.2 P _C -P _W	ry Flow PC 2	ring Fluid non	
P _w (psia) 1560.2	d Hydrocart	oons(1-e ^{-s})		cf/bbldeg(Fc	Q) ² e ⁻³)	Speci Speci P _c P _w 2	fic Gravit 659.2 P _C -P _W 318.7 789.5	ry Flow PC 2	ring Fluid name 752.9	
P _w (psia) 1560.2 141.2 1289.2	d Hydrocart	oons(1-e ^{-s})		cf/bbldeg(Fc	Q) ² e ⁻³)	Speci Speci Pc- Pw ²	fic Gravit 659.2 P _C -P _W ² 318.7 789.5	ry Flow PC 2	ring Fluid non 752.9 1. Pw Pc Pc 94.	
P _w (psia) 1560.2	d Hydrocart	oons(1-e ^{-s})		cf/bbldeg(Fc	Q) ² e ⁻³)	Speci Speci Pc	fic Gravit 659.2 P _C -P _W 318.7 789.5 1690.9 1942.5	ry Flow PC 2	ring Fluid men. 752.9 1. Pw Pc Pc 94. 85. 78.	
P _W 5 (psia) 1560.2 1411.2 1289.2 900.2 1428.2 PANY Gulf 011 ESS Box 766. IT and TITLE	Pt F	ons (1-e ^{-s})	(F _c Q) ²	cf/bbldeg. (Fc (1-	Q) ² e ⁻³) 2 1 1 2 n_0.694	Speci Speci Pc- Pw ²	fic Gravit 659.2 P _C -P _W ² 318.7 789.5	ry Flow PC 2	ring Fluid non 752.9 1. Pw Pc Pc 94.	
P _W E (psia) 1560.2 1411.2 1289.2 900.2 1428.2 PANY Gulf 911 PESS Box 766.	Pt F	ons (1-e ^{-s})	(F _c Q) ²	cf/bbl.deg.	Q) ² e ⁻³) 2 1 1 2 n_0.694	Speci Speci Pc	fic Gravit 659.2 P _C -P _W 318.7 789.5 1690.9 1942.5	ry Flow PC 2	ring Fluid	

INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

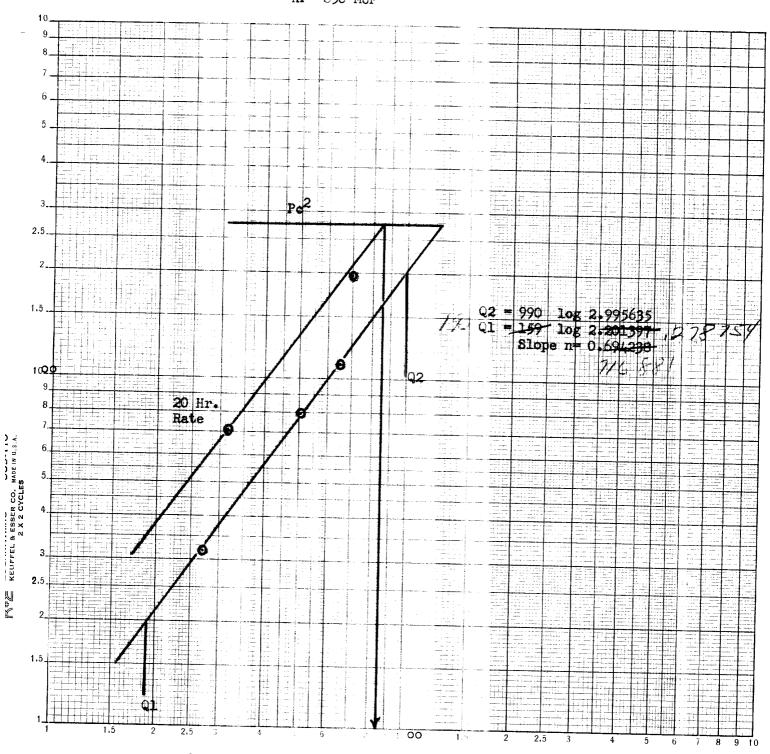
The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

NOMENCLATURE

- Q = Actual rate of flow at end of flow period at W. H. working pressure (P_W). MCF/da. @ 15.025 psia and 60° F.
- Pc 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- Pw Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- Pr Meter pressure, psia.
- hall Differential meter pressure, inches water.
- Fg Gravity correction factor.
- Ft Flowing temperature correction factor.
- Fpv Supercompressability factor.
- n _ Slope of back pressure curve.
- Note: If $P_{\mathbf{w}}$ cannot be taken because of manner of completion or condition of well, then $P_{\mathbf{w}}$ must be calculated by adding the pressure drop due to friction within the flow string to $P_{\mathbf{t}}$.

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Gulf Oil Corporation
Plains-Knight No.3
Unit L Sec.23, T24S, R37E
Fowler Paddock Gas
June 2-6, 1962
AP= 850 MCF



Q in MCF per Day

86 2777 1 1: 597 13

