

OIL CONSERVATION COMMISSION

Form C-122

WINTER BACK PRESSURE TEST FOR GAS WELLS

Revised 12-1-55

Pool Jalmat Formation Yates County Lea
Initial Annual Special X Date of Test 9-12/20-63
Company Dalport Oil Corporation Lease Winters C Well No. 1
Unit J Sec. 7 Twp. 25 Rge. 37 Purchaser El Paso Natural Gas Company
Casing 7 In. 22 I.D. Set at 3200 Perf. To
Tubing 2 3/8 In. 1.7 I.D. Set at 3285 Perf. To
Gas Pay- From 2796 To 2946 2796 xG .674 -GL 1884 Bar.Press. 13.2
Producing Thru: Casing X Tubing Type Well G. O. Dual
Date of Completion: 3-29-53 Packer 2950 Single-Bradenhead-G. G. or G.O. Dual
Reservoir Temp.

OBSERVED DATA

Tested Through (Prover) (Choke) (Meter)

Type Taps

| No. | Flow Data | | | | | Tubing Data | | Casing Data | | Duration of Flow Hr. |
|-----|-------------|------------------------|-------------|----------------------|-----------|-------------|-----------|-------------|-----------|----------------------|
| | (Line) Size | (Choke) (Orifice) Size | Press. psig | Diff. h _w | Temp. °F. | Press. psig | Temp. °F. | Press. psig | Temp. °F. | |
| SI | | | | | | | | 271 | | 72 |
| 1. | 1 | .750 | 134 | 2.25 | 84 | | | 241 | | 24 |
| 2. | 1 | .750 | 152 | 6.76 | 82 | | | 212 | | 24 |
| 3. | 1 | .750 | 162 | 10.89 | 80 | | | 183 | | 24 |
| 4. | | | | | | | | | | |
| 5. | | | | | | | | | | |

FLOW CALCULATIONS

| No. | Coefficient (24-hour Flg) | Pressure (psia) | Flow Temp. Factor F _t | Gravity Factor F _g | Compress. Factor F _{pv} | Rate of Flow Q-MCFPD @ 15.025 psia |
|-----|---------------------------|-----------------|----------------------------------|-------------------------------|----------------------------------|------------------------------------|
| 1. | 3.435 | 18.20 | .9777 | .9435 | 1.012 | 58.36 |
| 2. | 3.435 | 33.42 | .9795 | .9435 | 1.014 | 107.5 |
| 3. | 3.435 | 43.68 | .9813 | .9435 | 1.016 | 141.1 |
| 4. | | | | | | |
| 5. | | | | | | |

PRESSURE CALCULATIONS

Gas Liquid Hydrocarbon Ratio cf/bbl.
Gravity of Liquid Hydrocarbons deg.
P_c

Specific Gravity Separator Gas
Specific Gravity Flowing Fluid
P_c 284.2 P_c 80.8

| No. | P _w P _t (psia) | P _c | F _{cg} | (F _{cg}) ² | (F _{cg} Q) ² (1-e ^{-s}) | P _w ² | P _c ² -P _w ² | Cal. P _w | P _w P _c |
|-----|--------------------------------------|----------------|-----------------|---------------------------------|---|-----------------------------|--|---------------------|-------------------------------|
| 1. | 254.2 | 64.6 | 16.2 | | | | | 64.6 | 16.2 |
| 2. | 225.2 | 50.7 | 30.1 | | | | | 50.7 | 30.1 |
| 3. | 196.2 | 38.5 | 42.3 | | | | | 38.5 | 42.3 |
| 4. | | | | | | | | | |
| 5. | | | | | | | | | |

Absolute Potential: 256 MCFPD; n 910COMPANY Dalport Oil CorporationADDRESS 930 Fidelity Union Life Bldg. Dallas, TexasAGENT and TITLE GeologistWITNESSED Jack T. LittlefieldCOMPANY El Paso Natural Gas Company, Jal New Mexico

REMARKS

INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

NOMENCLATURE

- Q = Actual rate of flow at end of flow period at W. H. working pressure (P_w).
MCF/da. @ 15.025 psia and 60° F.
- P_c = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater.
psia
- P_w = Static wellhead working pressure as determined at the end of flow period.
(Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- P_t = Flowing wellhead pressure (tubing if flowing through tubing, casing if
flowing through casing.) psia
- P_f = Meter pressure, psia.
- h_w = Differential meter pressure, inches water.
- F_g = Gravity correction factor.
- F_t = Flowing temperature correction factor.
- F_{pv} = Supercompressability factor.
- n = Slope of back pressure curve.

Note: If P_w cannot be taken because of manner of completion or condition of well, then P_w must be calculated by adding the pressure drop due to friction within the flow string to P_t .