

Pool Jalnet Formation Yates County Lee  
Initial \_\_\_\_\_ Annual \_\_\_\_\_ Special X Date of Test 4, 22-26, 1957  
Company Southern California Pet. Lease Vosburg Well No. 1  
Unit I Sec. 18 Twp. 25 Rge. 37 Purchaser El Paso Natural Gas Company  
Casing 7" Wt. 23.0 I.D. \_\_\_\_\_ Set at 3168 Perf. 2792 To 2900  
Tubing 2 3/8" Wt. 4.7 I.D. \_\_\_\_\_ Set at 3321 Perf. \_\_\_\_\_ To \_\_\_\_\_  
Gas Pay: From 2792 To 2900 L 2792 xG 0.660 -GL 1843 Bar.Press. 13.2  
Producing Thru: Casing X Tubing \_\_\_\_\_ Type Well G. O. Dual  
Single-Bradenhead-G. G. or G.O. Dual  
Date of Completion: Dual: 4-6-53 Packer 3100 Reservoir Temp. \_\_\_\_\_

OBSERVED DATA

Tested Through (Pressure) (Gauge) (Meter) Type Taps Flange

| No. | Flow Data   |                |             |                      |           | Tubing Data |           | Casing Data |           | Duration of Flow Hr. |
|-----|-------------|----------------|-------------|----------------------|-----------|-------------|-----------|-------------|-----------|----------------------|
|     | (Line) Size | (Orifice) Size | Press. psig | Diff. h <sub>w</sub> | Temp. °F. | Press. psig | Temp. °F. | Press. psig | Temp. °F. |                      |
| SI  |             |                |             |                      |           |             |           | 358         |           | 72                   |
| 1.  | 4           | .750           | 201         | 4.64                 | 65        |             |           | 334         |           | 24                   |
| 2.  | 4           | .750           | 202         | 12.25                | 67        |             |           | 303         |           | 24                   |
| 3.  | 4           | .750           | 218         | 19.60                | 68        |             |           | 290         |           | 24                   |
| 4.  | 4           | .750           | 223         | 22.56                | 66        |             |           | 253         |           | 24                   |
| 5.  |             |                |             |                      |           |             |           |             |           |                      |

FLOW CALCULATIONS

| No. | Coefficient Flange (24-Hour) | $\sqrt{P_w P_f}$ | Pressure psia | Flow Temp. Factor F <sub>t</sub> | Gravity Factor F <sub>g</sub> | Compress. Factor F <sub>pv</sub> | Rate of Flow Q-MCFPD @ 15.025 psia |
|-----|------------------------------|------------------|---------------|----------------------------------|-------------------------------|----------------------------------|------------------------------------|
| 1.  | 3.435                        | 32.18            |               | .9952                            | .9535                         | 1.022                            | 107                                |
| 2.  | 3.435                        | 51.32            |               | .9933                            | .9535                         | 1.022                            | 171                                |
| 3.  | 3.435                        | 67.64            |               | .9924                            | .9535                         | 1.022                            | 224                                |
| 4.  | 3.435                        | 72.97            |               | .9943                            | .9535                         | 1.023                            | 243                                |
| 5.  |                              |                  |               |                                  |                               |                                  |                                    |

PRESSURE CALCULATIONS

Gas Liquid Hydrocarbon Ratio Dry cf/bbl.  
Gravity of Liquid Hydrocarbons \_\_\_\_\_ deg.  
F<sub>c</sub> 0.740 (1-e<sup>-s</sup>) 0.119  
Specific Gravity Separator Gas 0.660  
Specific Gravity Flowing Fluid \_\_\_\_\_  
P<sub>c</sub> 371.2 P<sub>c</sub><sup>2</sup> 137.8

| No. | P <sub>t</sub> (psia) | P <sub>t</sub> <sup>2</sup> | F <sub>c</sub> Q | (F <sub>c</sub> Q) <sup>2</sup> | (F <sub>c</sub> Q) <sup>2</sup> (1-e <sup>-s</sup> ) | P <sub>w</sub> <sup>2</sup> | P <sub>c</sub> <sup>2</sup> -P <sub>w</sub> <sup>2</sup> | Cal. P <sub>w</sub> | P <sub>w</sub> /P <sub>c</sub> |
|-----|-----------------------|-----------------------------|------------------|---------------------------------|--|-----------------------------|--|---------------------|--------------------------------|
| 1.  | 347.2                 | 120.5                       | 0.080            | 0.006                           | 0.0007   | 120.5                       | 17.3   |                     |                                |
| 2.  | 316.2                 | 100.2                       | 0.130            | 0.017                           | 0.0023   | 100.2                       | 37.6   |                     |                                |
| 3.  | 303.2                 | 91.9                        | 0.170            | 0.029                           | 0.0035   | 91.9                        | 45.9   |                     |                                |
| 4.  | 266.2                 | 70.9                        | 0.180            | 0.032                           | 0.0040   | 70.9                        | 66.9   |                     |                                |
| 5.  |                       |                             |                  |                                 |  |                             |  |                     |                                |

Absolute Potential: 300 MCFPD; n 0.615  
COMPANY Southern California Petroleum Corporation  
ADDRESS Box 1071, Midland, Texas  
AGENT and TITLE Joe A. Solomon, R.E., New Mexico, Engr. No. 2208  
WITNESSED Well tested by El Paso Natural Gas Company  
COMPANY Real-Solomon Engineering Company

REMARKS

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

- $Q$  = Actual rate of flow at end of flow period at W. H. working pressure ( $P_w$ ).  
MCF/da. @ 15.025 psia and 60° F.
- $P_c$  = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater.  
psia
- $P_w$  = Static wellhead working pressure as determined at the end of flow period.  
(Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- $P_t$  = Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- $P_f$  = Meter pressure, psia.
- $h_w$  = Differential meter pressure, inches water.
- $F_g$  = Gravity correction factor.
- $F_t$  = Flowing temperature correction factor.
- $F_{pv}$  = Supercompressability factor.
- $n$  = Slope of back pressure curve.

Note: If  $P_w$  cannot be taken because of manner of completion or condition of well, then  $P_w$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_t$ .

SOUTHERN CALIF. PETR. CO.  
 VOSBURG NO. 1  
 I - 18-25-37 LEA NM  
 4-26-1957

