

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☐ Initial ☐ Annual ☒ Special					Test Date 6-6-79	
Company CONTINENTAL OIL				Connection NONE		
Pool JALMAT				Formation YATES		Unit C
Completion Date 9-4-48		Total Depth 3000'		Plug Back TD —		Elevation 3107' GL
Farm or Lease Name SHOLES B-19						Well No. 2
Csg. Size 5 1/2"	Wt. 17 #	d 4.892	Set At 2700'	Perforations: OPEN HOLE From 2800' To 3000'		
Tbg. Size 2 7/8"	Wt. 6.5 #	d 2.441	Set At 2791'	Perforations: From OPEN To ENDED		Unit Sec. Twp. Rye. C 19 25S 37E
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE				Packer Set At NONE		County LEA
Producing Thru TBG.		Reservoir Temp. °F 80° @ 3000'		Mean Annual Temp. °F 60°		Baro. Press. - P _a 13.2
State NEW MEXICO						
L 2791'	H 2791'	Gg .718	% CO ₂ 1.07	% N ₂ 1.33	% H ₂ S .10	Prover 2"
Meter Run		Taps				

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
SI	(SINCE 9-18-61)						142		142	
1.	2"	X	.250"	30		92	125		125	1 HR.
2.	2"	X	.250"	40		98	118		118	(STABILIZED) 1 HR.
3.	2"	X	.250"	50		100	113		113	" 1 HR.
4.	2"	X	.250"	60		100	108		109	" 1 HR.
5.										

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	1.087		43.2	.9706	1.180	NL	54
2	1.087		53.2	.9653	1.180	NL	66
3	1.087		63.2	.9636	1.180	NL	78
4	1.087		73.2	.9636	1.180	NL	90
5.							

NO.	P _t	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio <u>DRY GAS</u> Mcf/bbl.
1.				NL	A.P.I. Gravity of Liquid Hydrocarbons <u>DRY</u> Deg.
2.				NL	Specific Gravity Separator Gas <u>.718</u> X X X X X X X X
3.				NL	Specific Gravity Flowing Fluid <u>X X X X X</u>
4.				NL	Critical Pressure <u>668</u> P.S.I.A. P.S.I.A.
5.				NL	Critical Temperature <u>398</u> R R

P _c <u>155.2</u>	P _c ² <u>24.1</u>	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.619$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.289$
NO.	P _t ²	P _w	P _w ²
1	19.1	138.2	19.1
2	17.2	131.2	17.2
3	15.9	126.2	15.9
4	14.7	122.2	14.9
5			

Absolute Open Flow <u>206</u> Mcfd @ 15.025		Angle of Slope θ <u>49.3°</u>	Slope, n <u>.860</u>
Remarks: <u>NO FLUID PRODUCED DURING TEST.</u>			
Approved By Commission:	Conducted By: <u>John C. Giddens</u>	Calculated By: <u>John C. Giddens</u>	Checked By:

NMOCD, HOBBS (2) - USGS, HOBBS (2) - FILE