

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 8/30/76	
Company Burleson and Huff				Connection None			
Pool Jalmat				Formation Yates		Unit P	
Completion Date 8/30/76		Total Depth 2900		Plug Back TD 2900		Elevation _____	
Farm or Lease Name Leonard		Well No. 1					
Csq. Size 5 1/2	Wt. 17	d _____	Set At 2900	Perforations: From 2707 To 2758		Unit Sec. Twp. Rge. P 20 25 37	
Tbg. Size 2 7/8	Wt. _____	d _____	Set At 2690	Perforations: From _____ To _____		County Lea	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 2690		State New Mexico	
Producing Thru Tbg.		Reservoir Temp. °F 100 @ calc. 2690		Mean Annual Temp. °F _____		Baro. Press. - P _a _____	
L 2690	H 2690	G _g 652	% CO ₂ _____	% N ₂ _____	% H ₂ S _____	Prover 2"	Meter Run _____
Taps _____							

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							391				72 hr.
1.	2	x	1/8	303		73	303				1 hr.
2.	2	x	3/16	260		74	260				1 hr.
3.	2	x	7/32	225		74	225				1 hr.
4.	2	x	1/4	200		75	200				1 hr.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	.2648		316.2	.9877	1.238	1.030	105
2.	.6082		273.2	.9868	1.238	1.026	208
3.	.8393		238.2	.9868	1.238	1.023	250
4.	1.087		213.2	.9859	1.238	1.020	289
5.							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.	.47	533	1.42	.943	dry	dry	.652	XXXXXX	670	375
2.	.41	534	1.42	.950				XXXXX		
3.	.36	534	1.42	.956						
4.	.32	535	1.43	.962						
5.										

NO.	P _c	P _w	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2}$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n$
1	404.2	163.38	113.61	1.465	1.465
2			84.87		
3			64.59		
4			51.86		
5					

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 423$

Absolute Open Flow	423 Mcfd @ 15.025	Angle of Slope θ	45°	Slope, n	1.000
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Remarks: _____

Approved By: _____ Conducted By: _____ Calculated By: _____ Checked By: _____