NEW MEXICO OIL CONSERVATION COMMISSION

| 1900 1004 | 4 . | ۲., | | Form C-12 | | |
|---------------|--------|-----|---|------------|--|--|
| *** * * * * * | to a d | | 2 | Form C-123 | | |

MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

| | | Jelmet | | Formation | Seven R | ivers- Q | ioen | _County | Lee | | |
|----------------|-----------------------------|---------------------|-------------------------------|---------------------------------|------------------|------------------|---------------------------------|--|------------------|-------------------------------|--|
| Initial Annual | | nuel | X | Spec | ial | <u>-</u> | Date of Test 3-24/4-1-60 | | | | |
| ompa | ny Cities | Service 0 | II Co. | ··· | Lease | Dabbs | | Well | L No | 1 | |
| nit | • | Sec23 | Twp . 25 | Rg | e. 37 | Purc | haser | El Paso Na | tural 0 | as Company | |
| asin | ng_7 | /t. 24.0 | _I.D. | .336 _{Se} | t at | le Pe | rf | r | ro | | |
| ubin | g Hone W | /t | _I.D | Se | t at | Pe: | rf | | °0 | | |
| as F | ay: From_ | 3090 To | 3361 | L | 1 449 x | .G 69 1 | | 1 692 I | Bar.Pres | ss. 13.2 | |
| rodu | cing Thru: | Casing | <u> </u> | Tu | bing | C:- | Type We | ell sing | le C | O Dual | |
| ate | of Complet | ion: 11-2 | 1-36 | Packe | r_ Non | • Sin | Reservo | oir Temp | 102 Es | t. | |
| | | | | | OBSERV | ED DATA | | | | | |
| e ste | d Through | XXXXXXX) | KEKKKE | Meter) | | | | Type Tap: | <u>Flan</u> | 90 | |
| | | Flow | Data | | | Tubing | Data | Casing Da | ıta | | |
|). | (Line) | (Choke) (Orifice |) | | + | | Temp. | | Temp. | Duration of Flow | |
| | Size | Size | psig | g h _w | o _F . | psig | ° _F , | psig | °F∙ | Hr. | |
| , | 4 | .750 | 119 | 4,50 | 73 | | | 134 | | 72 24 | |
| | 4 | .750 750 | 136 | 23.64 | 75 | | | 174 | | 24 24 | |
| : - | 4 | .750 | 158 | 2,25 | 66 | | | 159 | | 24 | |
| | | L | ! | | FLOW CAL | CULATION | 5 | | | | |
| | Coeffici | ent | I | Pressure | | | Gravity Factor | 1 - | | Rate of Flow Q-MCFPD | |
| | (24-Hou | · V | h _w pf | psia | F | t | $^{	extsf{F}_{	extsf{g}}}$ | Fpv | | 15.025 psia | |
| | 3.435 3.435 | 23 | 30 | 132.2 | .9877 | | 9318 | 1.012 | | 73.59 165.4 | |
| | 3.435 | | .04 | 141.2 | . 3850 | | 9318 | 1.014 | | 182.3 | |
| | 3.435 | 19. | .62 | 171.2 | .5543 | | . 9318 | 1.018 | | 63.55 | |
| | quid Hydro | oo ahaa Doo | tio Dr | | | ALCU ATI | ONS | | | 4 | |
| vit | y of Liqui | | | | cf/bbl. deg. | | Speci | fic Gravit fic Gravit 202.2 | | ng Fluid | |
| vit, | y of Liqui .4915 | d Hydroca: | rbons | | deg. | | Speci Pc P _w 2 | fic Gravit | Pc 40 | P _W P _C | |
| vit, | y of Liqui .4915 Pt (psia) | d Hydroca: | rbons (1-e ^{-s}) | (F _c Q) ² | deg. (F | (Q) ² | Speci Pc | fic Gravit | y Flowi Pc 40 | Pw Pc | |
| vit | y of Liqui .4915 | d Hydroca: | rbons (1-e ^{-s}) | 0.11 | deg. (F | (Q) ² | Speci Pc Pw2 | fic Gravit 202.2 P _C -P _W ² | y Flowi Pc 40 | Pw Pc 1972 | |

INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

NOMENCLATURE

- Q I Actual rate of flow at end of flow period at W. H. working pressure (Pw). MCF/da. @ 15.025 psia and 600 F.
- P_c = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- PwT Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- Pf Meter pressure, psia.
- hw Differential méter pressure, inches water.
- Fg Gravity correction factor.
- Ft Flowing temperature correction factor.
- F_{DV}^{-} Supercompressability factor.
- n I Slope of back pressure curve.

Note: If $P_{\rm W}$ cannot be taken because of manner of completion or condition of well, then $P_{\rm W}$ must be calculated by adding the pressure drop due to friction within the flow string to $P_{\rm t}$.