Revised 12-1-55

MULTI-POINT	BACK	PRESSURE	TEST	FOR.	GAS	WELLS
MODIT-LOTH!	DVOW		THOI	LOIL	unu	n

7OT	Lmat		F	ormation		Yates	J	_County_	Lea	
nitial				•	Spec	 ial_	Х			5-15-58
ompanySO	JTHERN	CAL. PI	et. Coi	RP.	Lease	Dabbs		We]		_
nit E										
sing 7								2		2828
bing 2										
ibing is Pay: Fi										
								-	_	
oducing T	ru: Ca	ising		Tul	oing	Sin	Type We gle-Brade	nhead-G.	G. or G	.O. Dual
te of Com	oletion:		·	Packe	none		Reservo	ir Temp.	-	
					OBSERV	ED DATA				
sted Thro	igh <u>(Pro</u>	over) (Choke)	(Meter)				Type Tar	s	
		Flow D	ata			Tubing	Data	Casing I		
(Prove	e) (Ori	fice)		. Diff.			Temp.	Press.	_	Duration of Flow
Size	· S	Size	psig	h _w	°F.	psig 478*	F.	psig	[⊃] F•	Hr.
4	.5	50 -	127.	22.09	80	129.2				24
			<u> </u>	<u> </u>			<u> </u>			
Coof	Cicient	+		ressure		CULATION		Compre	200	Rate of Flow
			「			tor	Factor	Facto		Q-MCFPD
	Hour)	√ h _w		psia	F. 9813	t	9498	F _{pv}	-	@ 15.025 psia
		72.5	-	+	• , , , ,			+		
1.5										
		<u> </u>								
				PR	ESSURE C	A CCITIATTO	ONS			
				PRI		ALCU ATI				66
Liquid Hy					cf/bbl.	ALCUATIO	Speci	fic Gravi	ity Sepa	rator Gas 66
s Liquid Hy	iquid Hyd	irocarb			cf/bbl.	ALCU ATI	Speci	fic Gravi	ity Sepa	rator Gas66
Liquid Hy	iquid Hyd	irocarb	ons		cf/bbl.	ALCU'ATI	Speci	fic Gravi	ity Sepa ity Flov PC 2	rator Gas 66
Liquid Hyvity of Liquid Pw	iquid Hyd 36	irocarb (ons 1-e ^{-s})	.12	cf/bbl. deg.		Speci Speci Pc	fic Gravi	P _C 2	ving Fluid
Liquid Hyvity of Light 9.9	iquid Hyd 36	drocarb (t F	ons		cf/bbl. deg.		Speci Speci Pc P _w 2	fic Gravi	rc 2	ving Fluid
Liquid Hyvity of Light 9.9	lquid Hyd	drocarb (t F	ons 1-e ^{-s})	.12	cf/bbl. deg.	alcuration	Speci Speci Pc	fic Gravi	rc 2	ving Fluid
Liquid Hyvity of Light 9.9	iquid Hyd 36	drocarb (t F	ons 1-e ^{-s})	.12	cf/bbl. deg.		Speci Speci Pc P _w 2	fic Gravi	rc 2	ving Fluid
Liquid Hyvity of Light 9.9	iquid Hyd 36	drocarb (t F	ons 1-e ^{-s})	.12	cf/bbl. deg.		Speci Speci Pc P _w 2	fic Gravi	rc 2	ving Fluid
Liquid Hyvity of Light 9.9	ia) 16.	o ² F	ons 1-e ^{-s})	(F _c Q) ²	cf/bbl.deg.	c ^Q) ² -e ^{-s})	Speci Speci Pc P _w 2	fic Gravi	rc 2	ving Fluid
Pw Pt (ps:	ia) 16.	o ² F	ons 1-e ^{-s})	(F _c Q) ²	cf/bbl.deg.	c ^Q) ² -e ^{-s})	Speci Speci Pc P _w 2	fic Gravi	rc 2	ving Fluid
Pw Pt (ps: 129.2	ia) 16.	2 F	ons 1-e ^{-s})	(F _c Q) ² A PETRO	cf/bbl.deg. (F) (1) MCFPD:	cQ) ² -e ^{-s})	Speci Speci Pc Pw2 16.2	P _c -P _w	rc 2	ving Fluid
Pw Pt (ps: 129.2 DESOLUTE POR DANY SODRESS P	ia) 16. cential: OUTHERN ILLE	ot F	ons 1-e ^{-s})	(F _c Q) ² A PETRO	cf/bbl.deg. (F) (1) MCFPD:	cQ) ² -e ^{-s})	Speci Speci Pc P _w 2	P _c -P _w	rc 2	ving Fluid
Pw Pt (ps: 129.2	ia) 16. cential: OUTHERN ITLE H. H	er locarb	ons 1-e-s)	(F _c Q) ² A PETRO	cf/bbl.deg. (F) (1) MCFPD:	cQ) ² -e ^{-s})	Speci Speci Pc Pw2 16.2	P _c -P _w	Pc 2	ving Fluid

*Unable to shut in well for shut-in pressure. Shut-in pressure for this test taken from the Deliverability test on the John M. Kelly, Shahan #3 dated 4-18-58.

** Average Jalmat slope of .771.

INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

NOMENCLATURE

- Q I Actual rate of flow at end of flow period at W. H. working pressure (P_W) . MCF/da. @ 15.025 psia and 600 F.
- P_c = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- Pw Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt- Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- Pf Meter pressure, psia.
- hw Differential meter pressure, inches water.
- FgI Gravity correction factor.
- F_t Flowing temperature correction factor.
- F_{nv} Supercompressability factor.
- n I Slope of back pressure curve.
- Note: If $P_{\mathbf{W}}$ cannot be taken because of manner of completion or condition of well, then $P_{\mathbf{W}}$ must be calculated by adding the pressure drop due to friction within the flow string to $P_{\mathbf{t}}$.